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### Teagasc, Moorepark, Fermoy, Co. Cork

Tel. 025 42222 Fax 025 42340

# Stack Emission Test Report

Monitoring objective: Sampling of Airflow

Monitoring deviations/ special requirements: Non

*Trial Ref* 20.002.4

Client Connollys Red Mills, 50115

Address Grange Lower, Goresbridge, Co Kilkenny . R95EKH4

Contact Name John Rea

Date of test 21/02/2020

Dryer Name Flaker 1, A2-5

**Powder Name** Animal Feed

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Authorised by Eoin.Murphy

Technical Manager

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**Airflow** 

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### 1.Executive Summary

*Trial Reference:* 20.002.4

Client: Connollys Red Mills,

Address: Grange Lower, Goresbridge, Co Kilkenny . R95EKH4

Date of test: 21/02/2020

IPPC Licence no: P1069-01
Emmission Limit: 50 mg/m³

Airflow of stack A2-5

on dryer Flaker 1, A2-5

The air flowrate was measured as 9,415 m of moist air

9,415 milder of moist air at 16 °C or

8,633 Nm³/hr of dry air under standard conditions, equivalent to

8,774 m³/hr under standard conditions on a wet basis (Note 2)

Notes:

1. Standard conditions are  $0^{\circ}$ C and 1013 mbar barometric pressure. The figures expressed as  $\pm$  mg/m³ are expanded uncertainty values (confidence level 95%).

We do not claim uncertainty values for results that are less than the limit of detection.

- 2. IPPC 4.2.1 expresses emissions under standard conditions on a wet basis for non-combustion gases. See comment at end of Explanatory Note.
- 3. This report refers only to the items identified herein.

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### 2. Method for monitoring Airflow to atmosphere

A series of velocity head readings are taken using a Pitot tube at intervals across the stack, from which the individual velocities at those points are calculated, The Pitot assembly for velocity measurement is mounted on the lance that is normally used for sampling air for particulates, together with a built-in thermocouple. A handheld datalogger reads the stack temperature (from the thermocouple), ambient temperature and barometric pressure. An Airflow type 5 manometer is used to take readings from the Pitot tube. Velocity measurement normally takes place along 2 sampling lines at right angles, according to EN 13284. The report gives total airflow on a wet and dry basis. The calculations are outlined in the Explanatory Note.

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# **Plant Conditions**

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Flaker 1 ,A2-5 Dryer:

A2-5 **Duct** 

Powder: Animal Feed

11:05:00 Start time End time 11:32:00

**Production Rate:** 3 tonnes/h

Feed Solid level: 86%

Product moisture: 14%

15°C Inlet temperature:

**Outlet Temperature** 16.6°C

Team Leader: **Donal Rawle** Sampled By:

Experimental officer

eoin.murphy

Research officer

Comment on plant conditions

Noise abatement in duct Normal Conditions

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Pitot Readings (see table below)

# Field Measurements

Stack: A2-5

Airflow Determination

Depth

0.69 m

Sampling side length

0.525 m

Per sample line

Pitot I No.	Readings (N/m²)	Edge Distance (m)	Sample Point	Sample line	Temperature of the tipe.
1	29	0.172	<b>✓</b>	1	25 96, 4t 2000
2	18	0.517	✓	1	1005 196.4
3	75	0.172	✓	2	10.6 16.6
4	69	0.517	✓	2 ctil	16.4
			consens	for its the	Herritan 16.6 Herritan 16.6 16.4

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# Field Measurements

Stack Temperature:	16.4 <b>°</b> C
Static Pressure (relative):	-14 <i>Pa</i>
Barometric Pressure (outside stack):	1001.0 <i>mbar</i>
Barometric Pressure (in stack):	1000.86 <i>mbar</i>

Dimensions (m	0.525 <b>X</b> 0.690		
Area (m²)	0.3623		
Velocity (m/s)	7.2		
Air Moisture (g/kg)	10		

### Air Flow

Mass flow 11,268 kg/h; 9,415  $m^3/h$  moist air (Note 3) 8,633 Nm3/h dry air

m³/h moist air under standard conditions, Note 4 8,774

Note 1: Stack temperature is an average of temperatures across sampling plane

Note 2: Flowrate was determined by subdivision of cross section area into anular rings in the case of a circular duct and rectangles in the case of a rectangular duct. The summation area accounted for

was 0.3623

Note 3: At stack conditions, density 1.1968 kg/m³

Note 4: Moist air volume under standard conditions as per 4.2.1 of IPPC for non-combustible gases.

Note 5: No wall effect factor applied.

Note 6: Velocity and flow are determined from the sample points

### Sampling

Max/Min Ratio of pitot readings Ratio < 9:1 OK 0.0 % Isokinetic ratio

Leak Test < 2%

Ambient temperature °C Weight of water collected g in moisture trap

### **Comment on Sampling:**

Angle of flow normal (<15°)			

#### **Airflow**

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## 6. Explanatory note on Stack Emission Report for Total Particulate

1. The average air velocity **v** is calculated as follows:

A cross-sectional area  $\mathbf{a_i}$  is associated with each point, where a Pitot reading is taken and where air is sampled for particulate. The velocity  $\mathbf{v_i}$  in each segment is calculated as a function of the Pitot pressure and the temperature. The flow  $\mathbf{a_i}$  through each segment (associated with each point of measurement) is calculated as:

$$\mathbf{q_i} = \mathbf{a_i} \cdot \mathbf{v_i}$$
  $[\text{m}^3/\text{s}]$ 

The total flow of moist air,  $\mathbf{Q} = \sum \mathbf{q_i}$  [m<sup>3</sup>/s]

and the average velocity,  $\mathbf{v} = \mathbf{Q}/\mathbf{A}$ , [m/s]

where **A** is the cross-sectional area of the stack, e.g.  $\mathbf{A} = \pi \left( D/2 \right)^2$  for a circular stack.

- 2. Air density for moist air is determined from first principles as a function of temperature, pressure and water vapour content. The relationship between volumetric flow of moist air in duct,  $\mathbf{Q}_h$  [m³/h], massflow of moist air in duct,  $\mathbf{m}_h$  [kg/h], and flowrate of dry air in duct under reference conditions,  $\mathbf{Q}_{nh}$  [Nm³/h], is:
- a. Flowrate per hour (m³/h):  $\mathbf{Q_h} = 3600 \ \mathbf{Q}$ , where Q is in (m³/s)
- b. Mass flowrate (kg/h):  $\mathbf{m}_h = \mathbf{Q}_h \boldsymbol{\rho}$ , where  $\boldsymbol{\rho}$  = the density of air at the actual temperature, pressure and moisture in the stack.
- c. To convert from volumetric flow of moist air to moist air under standard pressure and temperature:

$$Q_{mh} = Q_h \times \frac{P_s}{1013} \times \frac{273}{273 + T_s}$$

d. Convert from volumetric flow of moist air of dry air under standard conditions:

$$Q_{nh} = Q_h \frac{(100 - B_{ws})}{100} \times \frac{P_s}{1013} \times \frac{273}{273 + T_s}$$

where  $\mathbf{B}_{ws}$ = air moisture in % v/v (= Air Moisture in g/kg x 0.151). Air Moisture in g/kg is determined from the weight of moisture absorbed by the desiccant [g] and the volume of sampled air recorded by the gasmeter and converted to mass [kg], as follows

Mass of dry air at reference conditions, 
$$M_{ad0} = \frac{V_m \times 273}{T_m + 273} \times \frac{P_m}{1013} \times \rho_0$$
 [kg]

where  $P_m$  = barometric pressure at gasmeter [mbar].

Humidity ratio, 
$$x = \frac{W_w}{M_{ad0}}$$
 [g/kg of dry air]

where  $w_w$  = weight of water absorbed by desiccant.

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3. A gasmeter is used to measure the sampled air volume. Measured concentration of particulate is:

 $c = w \times 1000/V_{mo}$  [mg/Nm<sup>3</sup>], where w is total weight [g] of dried sample (including washings) and  $V_{mo}$  is the cumulative flow of sampled air measured by the gasmeter, corrected for temperature and pressure.

The total loss **L** [kg/h] is calculated as **c** times the estimated flowrate of dry air in the stack at standard conditions (0°C and 1013 mbar), divided by  $10^6$  for unit conversion (mg to kg).

4. Isokinetic ratio is calculated as  $100 \times V_{mo}/V_{no}$  %, where  $V_{no}$  is the target cumulative flow of dry air at the sampling nozzle during sampling, calculated from the Pitot readings P as  $0.84\sqrt{(2P/\rho)}$  for an S-type Pitot tube, and corrected for moisture removal, stack temperature and pressure to standard conditions. The isokinetic ratio should be between 95 and 115% for total particulate.

#### 5. Summary of notation:

- **A** Cross-sectional area of the stack  $(=\pi(D/2)^2)$  for a circular stack of diameter D).
- a Sampling nozzle cross sectional area
- **a**<sub>i</sub> Cross-sectional area is associated with each point.
- $\mathbf{B}_{ws}$  Water vapour content on a volumetric basis, i.e. volume of water vapour / volume of moist air.
- **c** Gravimetric dust concentration [mg/Nm<sup>3</sup>]
- **ELV** Emission limit value

GasmeterCF. Gasmeter calibration factor

- L Total loss [kg/h] i.e. estimated mass of powder being lost in stack
- $\mathbf{m_h}$  Total mass flowrate of air in stack [kg/h] =  $Q_h \rho$
- P Pitot tube reading, Pa
- $P_s$  Barometric pressure in stack, mbar.  $P_m$  = barometric pressure at gasmeter
- **Q** Total airflow in stack =  $\sum \mathbf{q_i}$ , m<sup>3</sup>/s
- $\mathbf{Q_h}$  Total air flow per hour [m<sup>3</sup>/h] = 3600  $\mathbf{Q}$
- $\mathbf{q_i}$  Flow associated with each point =  $\mathbf{a_i} \mathbf{v_i}$
- Q<sub>mh</sub> Total air flow expressed as moist air corrected for standard pressure and temperature [m<sup>3</sup>/h]
- $\mathbf{Q}_{\mathbf{n}\mathbf{h}}$  Total air flow expressed as normal cubic metres (dry air) per hour  $[\mathrm{Nm}^3/\mathrm{h}] = \mathbf{m}_{\mathbf{h}}/\mathbf{\rho}_{\mathbf{0}}$
- t Sampling duration
- $T_m$  Gasmeter temperature (°C);  $T_s$  Stack temperature, °C
- v Average air velocity = Q/A
- **v**<sub>i</sub> Velocity at any point (function of the Pitot pressure and the temperature).
- **v**<sub>s</sub> Mean velocity at the sampling points
- $V_{\rm m}$  Volume of air measured by gasmeter (m<sup>3</sup>),
- $V_{mo}$  Cumulative flow of sampled air measured by the gasmeter, corrected for temperature and pressure (Nm<sup>3</sup>).
- $V_{no}$  Target cumulative flow of dry air at the sampling nozzle during sampling, calculated from the Pitot readings and corrected for moisture removal, stack temperature and pressure to standard conditions (Nm<sup>3</sup>).
- $\mathbf{w}$  Sample weight;  $\mathbf{w}_{\mathbf{w}}$  weight of water absorbed by desiccant
- x Humidity ratio (g/kg of dry air)
- ρ Density of air at the actual temperature
- $\rho_0$  Density of dry air = 1.2928 kg/m<sup>3</sup> at standard conditions (0°C, 1013 mbar)

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