

CIR20 - 130

REV: 02

**Biostabilisation Plant Biofilter
Management Plan
CIR20-130**

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Originator

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Date Released.....

Purpose

Outline Biofilter Management

Scope

Biostabilisation Plant

Reason For Issue

First Release

Responsibility

Operational Director

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Biofilter Management

Moisture content, pressure, flow reduction, temperature, pH, porosity and condition of the filter material are parameters that need to be monitored at intervals. The moisture content and organic matter content should be measured semi-annually; back-pressure, temperature, and pH should be monitored monthly. Prompt attention to any abnormalities will prevent the possibility of any odours being released to the air-stream. pH should be maintained in a range of 6-8.

The effectiveness of the biofilter can be measured empirically by sampling differential air pressure at the airline access port between the biofilter and the blower module. If there is significant back -pressure or restricted airflow, it can be an indicator of too much compaction of the media. Caution should be exercised in this regard, as channelling and cracking of the media may create air short-circuit zones, making the air pressure test unreliable. As a general rule, completely replace the material every 12-18 months to compensate for volume reduction and prevent the development of cracks or channels that allow air to escape without treatment. If the biofilter is working properly after six months and settling is observed, adding an additional layer of biofilter media to the top of the media may be indicated. The CCS biofilter is designed for easy replacement of the filter media on a preventative maintenance basis. Simply replacing the filter media can compensate for a variety of biofilter failure issues including drying, over-saturation, cracking, settling or compaction.

The material needs to be kept at 50-60% moisture, and if it is too high, simply drain the excess moisture or re-mix the media, adding dry material as is necessary. A drain and collection port is provided in the biofilter. The maintenance of a good moisture level in the biofilter also guards against the development of cracks.

The biofilter surface within the canopy should be observed at monthly intervals when moist air can be observed escaping the filter. The moisture-laden air should be discharging evenly through the surface of the biofilter. A zone with no exhaust air escaping suggests a possible channelling or compaction problem. Since air will follow the path of least resistance, a zone with excess air discharge may also indicate a problem. Overly dry or moist surface areas are also indicators of uneven airflow. Short-circuiting of air requires complete re-mixing or replacement of the filter media as a preventative measure against the release of untreated air.

The microbes, which are most effective for odour removal, are sensitive to acidity in their environment. The nitrification of high quantities of ammonia within the biofilter can acidify the filter material. Therefore, the pH of the filter should be measured frequently at several locations and depths using the same samples and methodology for determining moisture. If the pH drops below the recommended level, lime or wood ash can be added to restore neutrality or the material can be exchanged with fresh media.

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A substantial decrease in organic matter content may indicate that some or all of the filter material needs to be replaced, particularly if the filter material is compost-based. Again, the filter material can be replaced with fresh material. The organic material in the biofilter has a tendency to settle. In the event that this settling exceeds 6 inches, replace the filter media back up to the initial level. After one or two new layers of fresh media have been placed on top of the biofilter, it may be time to replace the entire biofilter media as a preventative measure. Finally, periodically check for odours. In the event of off-odours being present, replace the material.

Provided the above parameters are monitored frequently and maintained within the recommended ranges, the biofilter will operate at maximum air-contaminant removal efficiency.

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**Biostabilisation Plant Odour
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Outline Odour Mangement Plant for Biostabilisation Plant

Scope

Biostabilisation Process

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Building Ventilation and Odour Abatement

While the building is designed to be operated under slight negative pressure (1-4 air changes per hour), the air handling design for the building has been developed to minimize the volume of air to be handled and consequently the biofilter size:

The management of all raw bio-waste through the dry fermentation results in all emissions from this process to be directed to the CHP. The consequential thermal oxidation of the anaerobic exhaust will give >99% reduction in odour from the material while being maintained under anaerobic conditions.

The uncontaminated air space above the tunnels and fermenters is isolated from the main building to avoid the requirement to biofilter this void space. This is ventilated directly to atmosphere with no consequential odour risk.

The interior of the building is coated with a polyurethane coat for corrosion protection and also to seal the building so that a low to moderate air exchange rate can be facilitated without risk of fugitive emissions.

As all of the composting process occurs within sealed biocells and tunnels with a low head space, air re-circulation is applied to minimize exhaust generation and thus reduce the biofilter load.

As a result, the ventilation of the main building void is designed for 1-4 air changes per hour. This will allow for rapid clearance of any fog from the building during material movement between biocells/tunnels and screening while minimizing fugitive emissions from the building. This air is mixed with hot and humid exhaust from the aerobic tunnels passed through the biofilter to reduce the odour output from the facility down to levels in compliance with the EPA license and to ensure that sensitive receptors are not impacted by the facility's operation.

The odour abatement system consists of the compost aeration system described previously, the building ventilation system including ventilation piping installed in the roof space of the reception/process building, ventilation blowers, enclosed biofilter and discharge stack. The ventilation pipe work is located in the roof spaces and operates under vacuum. The piping and blowers are sized to ensure that between 1 and 4 air changes per hour can be applied to the building void. The exhaust from the composting vessels will be initially passed through the mixing chamber where the air stream will be mixed with the humid exhaust from the tunnels. This mixture will combine to create a humid exhaust with a moderate temperature that will be suitable for biofiltration. The subsequent exhaust will be passed through a biofilter bed that is composed of graded wood chip. This media has been found to provide good odour removal efficiencies. The biofilter has been designed to allow an empty bed retention time (EBRT) of between 45 and 90 seconds.

In the event of desiccation of the media, the biofilter can operate in bio-trickling mode. In this mode, the organic media is kept permanently moist through the use of sprinklers. The biofilter has a bed volume of 1,000 m³ and the exhaust from the biofilter is then discharged through a stack to the atmosphere. The stack is 6.5m high with a internal diameter of 1.7m.

The full enclosure of the facility with a single discharge point allows for maximum control of the odour output from the facility. The combination of enclosure, optimised compost aeration,

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effective air stream capture and treatment will result in odour emissions from the facility that will not result in nuisance in the vicinity of the facility. One of the primary design criteria for the facility is its odour impact and the above five elements are being developed in parallel with an odour model that will ensure that the odour emission limits set in the EPA license (Table 1) are not exceeded.

Table 1: Emission Limits Values for Biofilters (EPA License)

Parameter	Emission Limit Value
Ammonia	50 ppm (v/v)
Hydrogen sulphide	5 ppm (v/v)
Mercaptans	5 ppm (v/v)

Table 2. Biofilter Parameters

Parameter	Min	Mean	Max
Volume of Air/day m ³	370,000	900,000	1,776,000
Volume of Air/hour m ³	1,540	37,500	75,000

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Odour Management Plan

The Odour Management Plan (OMP) is a core document that is intended to detail operational and control measures appropriate to management and control of odour at the site. The format of the OMP should provide sufficient detail to allow operators and maintenance staff to clearly understand the operational procedures for both normal and abnormal conditions.

An Odour Management Plan (OMP) should be prepared for all processes. The OMP should also include sufficient feedback data to allow site management (and local authority inspectors) to audit site operations. An example of some of the issues to be considered is summarised as follows. More detailed guidance is provided with this document.

A summary of the site and Composting facility, odour sources and the location of receptors,

Details of the site management responsibilities and procedures for reporting faults, Identifying maintenance needs, replenishing consumables, complaints procedure,

Odour critical plant operation and management procedures (e.g. correct use of plant, process, materials; checks on plant performance, maintenance and inspection

Operative training,

Housekeeping,

Maintenance and inspection of plant (both routine and emergency response),

Spillage management procedures,

Record keeping – format, responsibility for completion and location of records,

Emergency breakdown and incident response planning including responsibilities and mechanisms for liaison with the local authority

Public relations.

The Odour Management Plan is a living document and should be regularly reviewed and upgraded. It should form the basis of a document Environmental and Odour Management system for the operating site. The Odour Management System documentation should define the roles of the Plant Operator and staff and sets out templates in relation to the operating of the facility and reporting procedures to be employed. Requirements for the Odour management plan should be implemented thought out the site with a branched management system implemented in order to share responsibility around the site. The head manager should ensure all works are performed in accordance with the OMP. The OMP will be integrated in the overall Environmental Management System/Performance management system. The following principals should be followed:

The Composting Facility building will be sealed on all inner surfaces to ensure high building skin integrity. Traditional cladding techniques (either double skin or single skin with joints taped and flexi sealed) will have an approximate leakage volume of 10 to 30 m³ air per m² of clad surface area. This will be prevented during the new build.

The access doors of the Facility will be fitted with rigid rapid roller doors with an opening speed of 2.6 m/s minimum. Each door will also be fitted with a high efficiency air curtain.

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Computational fluid dynamic modelling performed on a similar facilities has demonstrated greater than 90% containment efficiency on open doors. Coupled with the negative air extractions system, it is anticipated that no odours will escape through door openings.

The Composting Facility odour management system will allow for gas extraction from individual zones within the composting process. Independent negative air extraction will be provided to the first and second stage composting processes, waste reception hall and finished compost and screening hall.

The significant odourous processes within the Composting Facility will be doubly contained and negatively ventilated to two stages of odour control. The first and second stage composting tunnels will be enclosed within their own enclosed structures within the sealed building. This will prevent the release of high strength odours to the headspace of the building. Furthermore, this significantly reduces the risk of odour escape from the building and provides significant comfort in terms of odour minimisation and management.

The odour control system will consist of a biofiltration system that will operate in biotrickling mode which will ensure all contaminants that could build up within a traditional fixed phase biofiltration system will be minimal as contaminants will be washed from the biofiltration bed media.

The proposed air introduction plenum for the biofiltration system is based on proven air introduction techniques. The air introduction plenum will be divided into 4 separate cells to allow for the zoned treatment of odours within the biofiltration system.

The recirculation system for the biofiltration system will allow for the focused addition of essential nutrients and minerals to ensure high microbial activity within the biofiltration bed medium.

The proposed plenum floor is designed with equal air distribution in mind to ensure homogenous flow through the biofilter bed.

The odour control system will be fitted with sensors and monitoring analysers to allow for preventative maintenance and alarm tagging through the SCADA system. In addition, hours of operation will be recorded and preventative maintenance will be scheduled on a runtime basis as recommended by the equipment manufacturers.

All rough debris and organic matter will be cleaned from the surface of the waste reception hall floor at the end of each day's operation. This will be recorded into a check sheet and incorporated into the overall odour management plan.

All surfaces contaminated with odourous material will be washed down as required as part of the clean up schedule for the waste reception hall and finished compost screenings hall. This will be recorded into a check sheet and incorporated into the overall odour management plan.

No putriscable waste will be stored outdoors at any time. All operations will be carried out indoors.

Training and pre planned maintenance works will be organised using a check sheet approach. All staff will be trained in the execution of the Odour management plan. An annual check sheet will be used to ensure preventative maintenance is performed upon the odour management system for the Composting Facility.

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Standard Operating Procedures

Odour abatement/minimisation systems are installed with the aim of mitigating odours from the particular process(s). In some circumstances odour abatement system can become significant sources of odour especially if sufficient treatment is not being achieved. For example, insufficient treatment could be associated with system failure, poisoning of media, exhaustion of media, insufficient gas removal volume, broken covers, open hatches etc. There is a tendency in many facility environments that when an odour control system is installed it requires very little system checking especially if SCADA controlled. A simple management system incorporated into site operations can significantly reduce the risk of odour control plant failure and also provide a valuable picture for operations and maintenances schedules.

The overall odour control plant management system will vary for various technologies. For the proposed composting facility upgrade, the following odour control/minimisation plant could be installed to control odours emanating from specific processes within the plant. These include:

Biofilters

Extraction ductwork located throughout Composting facility,

Dissolved oxygen probes in aerated composting process.

For each of the odour control technologies, an operational verification procedure should be performed from actually visiting each piece of equipment. For sensitive mechanical odour control plant, such as chemical scrubbers, biotrickling filters and biofilters, a daily check should be performed. Small changes in operational parameters could lead to significant emission of odours.

For odour control/minimisation plant such as odour control ductwork, covers etc., which are less susceptible to breakdown (i.e. since there are little mechanical moving parts), a weekly check should be performed.

All system checks should be document controlled and available for viewing by odour complaints verification personnel, chief maintenance personnel and plant manager. Response/Action plans should be established for system repair where by a repair team trained in the operation and maintenances (O&M) of this specific plant are available to perform dedicated repair. O&M manuals should always be available and a spares inventory should be maintained for essential spares.

Any recording of system performance should be compared to design specification and performance as outlines within a P&ID flow diagrams developed for the built site.

Table 3 illustrates a typical odour control plant daily/weekly checking procedure for odour abatement plants such as chemical scrubber, dry chemical scrubbers and flares. Certain parameters such as subjective and objective assessment checks (airflow rate, static/differential pressures etc) should be performed daily while other parameters such as odour threshold concentration should be performed quarterly which is in keeping with EPA recommendations for similar facilities. Table 9.3 illustrates a typical odour minimisation plant system checking procedure for impermeable covers, odour control ductwork, pressure release valves etc.

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Table 3.1. Odour Control Unit (OCU) checking procedure and recording.

Odour Abatement equipment process data sheet			
OCU name		Location (NE coordinate)	
OCU P&ID ref. No.		Time of check (24 hr)	
Date of check:		Commissioning date:	
QA/QC by:		Next service date:	
Supplier and contact details:			
Emergency contact No.			
OCU description			
Notes:			
Process description			
SENSOR CALIBRATION DATES			

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Chemical/BTF/Carbon	Liquid flow sensor	
Chemical/BTF/Carbon	Differential/static pressure	
Chemical/BTF/Carbon	Temperature	
Outlet stack-composting	Mercaptans	
Outlet stack-composting	Ammonia	
Outlet stack-composting	Amines	
Outlet stack-composting	Hydrogen sulphide	
Notes:		
Subjective process verification		
Is the fan running and sounding OK (Y/N comments)?		
Is liquid recirculating within the recirculating line of the biofilter (Y/N comments)? Please record value		
Is dump liquor flowing freely from overflow sump (Y/N comments)?		
Is liquid distributed equally over packing media and is there evidence of settlement in biofilter/scrubbing media (Y/N comments)?		
Is recirculating liquor clear or cloudy (Y/N comments)		
Are all liquid distribution nozzles/gate clear (Y/N comments)		
Notes:		

Table 3.2. Odour Control Unit (OCU) checking procedure and recording.

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Objective process verification					
Parameter	Average	Min	Max	Design value as per P&ID	Action
Air flow rate (m ³ /hr)					
Temperature (°C)					
Inlet ductwork Static pressure (mm WG)					
Differential pressure across system components (mm WG)					
Inlet dust load (mgN/m ³)					
Odour character: (Descriptor)					
Notes:					
Treated airflow	Average	Min	Max	Design value as per P&ID	Action
Airflow rate (Nm ³ /hr)					
Temperature (°C)					
Outlet static pressure (mm WG)					
Outlet odour conc. (Ou _E /m ³)					
CEMS outlet conc. (mg/m ³)					
Outlet odour emission rate (Ou _E /s)					
Outlet odour character: Descriptor					

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Irrigation recirculation	Average	Min	Max	Design value as per P&ID	Action
Recirculation flow (m³/hr)					
Temperature (°C)					
Conductivity (s)					
PH (0 to 14)					
Redox if appropriate (mv)					
Stability on Redox/pH historically					
Irrigation drainage	Average	Min	Max	Design value as per P&ID	Action
Dump volume (m³/hr)					
Conductivity (s)					
Batch dumping frequency (weeks)					

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Table 3.3. illustrates a typical odour minimisation equipment system weekly checking procedure for odour control ductwork, etc.

Odour Abatement Plant process data sheet			
Equipment name		Location (NE coordinate)	
Equipment P&ID ref. No.		Time of check (24 hr)	
Date of check:		Commissioning date:	
QA/QC by:		Next service date:	
Supplier and contact details:			
Emergency contact No.			
Equipment description			
Notes:			
Process description			
Item description	Parameter	Compliant/Actions	
Ductwork	Static pressure P&ID location No 1		
	Static pressure P&ID No location 2		
	Static pressure P&ID No location 3		
	Static pressure P&ID No location 4		
Volume control dampers (VCD)	P&ID No. 1 Damper setting/head loss		
	P&ID No. 2 Damper setting/ head loss		
	P&ID No. 3 Damper setting/ head loss		
	P&ID No. 4 Damper setting/ head loss		

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are all condensate drip points free flowing and unblocked?	
Notes:	

The implementation of such quality checking procedures will provide both system confidence and preventative maintenance thereby reducing any risk associated with odour control/minimisation equipment.

The frequency and planning of sampling depend on the type of process. When the parameters are expected to develop gradual trends like dry chemical scrubbers rather than sudden changes like chemical scrubbers, the frequency of checking can be low (monthly, biweekly). If the system is more susceptible to cyclic loads, weekly or even daily monitoring may be required, depending on the history and the consequences that may arise from not realising an issue. More importantly seasonal changes in odour loads on plant and equipment can affect the overall performance of the system and combined with the behaviour of people on the receptor side during changing weather conditions (i.e. warm summer days could result in higher odour loads due to higher metabolic activity of bacteria coupled with people enjoying outdoor activities, etc.) For some processes, continuous monitoring may be useful, especially when the consequences of failure are significant. Risk assessment of plant failure is important to define key operational and maintenance parameters for the odour control unit (OCU). On the basis of this risk assessment measures can be defined to reduce the probability of high consequence events or to mitigate their impact.

The public will remember unscheduled emission episodes with great tenacity. It is therefore important to not fully rely on the environmental performance of odour mitigation under normal operational conditions but also consider them under unscheduled emission events. It is therefore crucial to consider and manage risks of odour emissions during:

Odour Control Unit (OCU) commissioning,

Start-up and shutdown of odour abatement units with consideration for duty standby on particularly odour processes (i.e. this has been implemented into the design),

Management of highly odorous materials

OCU servicing, and unscheduled shutdown,

In assessing these risks, it must be taken into account that response to odours is almost immediate. In order to manage these odour detection and complaint risks, a number of actions may be considered:

Plan high-risk activities in periods where receptor sensitivity to annoyance is low like during wet weather when they are indoors, or during colder winter months, or during early morning/late evenings during periods of low atmospheric turbulence, etc.

Consider providing standby capacity, etc. If all else fails, inform potentially affected residents of the probability of temporarily increased odours and explain potential benefits due to these increases (i.e. maintenance of OCU, etc.)

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**Biostabilisation Plant
Maintenance Plan
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Purpose

Outline a Maintenance Plan for the Biostabilisation Plant

Scope

Biostabilisation Plant

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First Release

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Maintenance methodology

Site Tidiness

It is vitally important to keep the AD/compost facility as a whole clean and tidy. In particular, it is important that any remaining organic waste that is left on the ground after delivery and mixing should be swept up and placed in a tunnel. This is specifically important in relation to the combined MBT / source separated nature of the facility. Periodically a general clean up of the traffic area will be required to remove accumulated sediment. Litter should also be removed before it accumulates. This should occur on a daily basis. If possible, water must never be allowed to stand on the impervious surfaces as these can be sources of odour. All such recommendations, actions, or problems shall be noted on the operator's daily log.

Tunnel & Fermenter Maintenance

Biogas Handling and other Fermenter System maintenance

The biogas system (piping & gas storage bag) should be maintained in accordance with the operations manual. Specific care should be taken in relation to leak detection and correct operation of the valves and gas blowers to ensure effective clearance of the fermenters of biogas and CHP feed. The percolate system will also require regular inspection to ensure that no blockages occur and that any build up of deposits within the lines are avoided.

CHP maintenance

This is critical to the effective operation of the plant and all oil and filter changes should be conducted at the specified intervals. Gas quality analysis is particularly important to avoid corrosion of the engine by sulphide and siloxanes in particular.

Door maintenance

The large flexible door will flex to a degree during use. The sliding tunnel door brackets should be checked for alignment periodically and adjusted accordingly due to potential slippage. Proper man-lift equipment should be used when adjusting the higher brackets. Gaskets and seals on the doors and roofs of the tunnels should be inspected for wear and a proper seal each time the tunnels are loaded and unloaded. Foreign debris such as wood chips or compost should be scraped off the seal before the door is closed.

Blower Maintenance

While manufactured from stainless steel they will suffer form abrasion. The blowers are also subject to corrosion and degradation or damage from foreign particles. Through the access port on the blower, the inside compartment of the blower is to be visually inspected every three months for wear, damage and/or the build up of scum. Upon turning off the blower and locally isolating it, the operator will look inside the blower area and observe the fan blade and housing. The fan should not be cracked, bent, or otherwise damaged. There may be some normal wear such as small dents and other signs of abrasion. This is not a serious concern as long as the blower is still working properly and not imbalanced. The blower should be listened to closely during the start and stop cycle for signs of fan blade imbalance. Should the fan be unbalanced, broken, or damaged, it should be replaced as soon as possible.

The most common cause of blower failure is water ingress into the motor housing that causes a short-circuit. The blowers in Clean Ireland will be fitted with water and oil shaft seals and the shaft is kept under suction to prevent moisture discharge to the motor. However, in the event of motor failure, CCS should be contacted and a maintenance team will visit the site to change out the motor. Typically, only one blower is likely to go down at any time. In this event, the tunnel

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can be kept running by linking the remaining blower directly to the tunnel floor duct by flex hose and operating the system under vacuum to maintain aerobic conditions. This is important in the event of a delay in repairing the damaged blower.

Valve and Pipe Maintenance

The air reversal valves are made of stainless steel and should not be subject to corrosion. The valve should be checked regularly for blockages and build up of scum and washed down accordingly. Flex hose joining the pit pipes should be removed regularly and the pipes checked for blockages. If blockages occur then the pipe should be disconnected at the joint with the actuator valve and the pipe washed out and allowed to drain. The motor on the flow reversal valve may require replacement at intervals. The HDPE pipe work and fittings should require minimum maintenance. However, the flex hose may become brittle over time and will need replacement.

Temperature Probe Maintenance

Check the temperature probes each time they are removed for bends, cracks or breakage. The interior of the head compartment should be checked for corrosion and / or moisture accumulation. Calibration will be required to comply with the ABPR license conditions. This can be arranged with CCS.

Leachate and Condensate Collection System Maintenance

The leachate valve should be inspected visually every week to ensure that it is following the correct open and close sequence. Upon inspection, isolate the valve, open manually and check for blockages. It is critical that this valve is kept clear to avoid leachate build up in the pipe work.

Maintenance of Concrete Structures

As with any concrete structure, be it a road, bridge or pavement, ongoing maintenance will be required to assure that wear and tear from day to day operations does not compromise the integrity of the infrastructure and reduce the plants 60 year working life span. It is recommended that the client instruct a building surveyor to undertake an annual inspection of the facility. Particular attention should be paid to areas where the tele-handler makes frequent contact with the infrastructure. These areas should include the floor to wall interface in the tunnels, the internal roof infrastructure and the lower areas of the maturation pad push walls. Furthermore, any damage that might result at times outside of these inspections should be surveyed and the engineers called if appropriate. The engineer should then be able to specify appropriate works, repairs or products to assure that any areas of damage do not affect the integrity of the facility as a whole.

Loader Maintenance

As per manufacturer's recommendations.

Mixer Maintenance

As per manufacturer's recommendations.

Trommel Screen Maintenance

As per manufacturer's recommendations.

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Maintenance Check List

Component	Estimated Life Span	Action	Frequency
Reception building			
Pressure washer	3-4 years	See manufactures specifications	
Roller shutter doors	7-10 years	As manufactures specifications	Monthly
Tunnels			
Tunnel /Fermenter integrity	20 years	Inspect all high impact areas, report any abnormal signs or high wear to the appointed structural engineer	Per Batch
Fermenter door	+10 year	Check door and roof seals for obstruction, wear and proper seal	Weekly
Tunnel door	+10 year	Check door support and rail alignment	Monthly
Tunnel door wagon	+10 years	Check for position and tightness of door buffer	Monthly
Tunnel/ Fermenter grates	2-5 years*	Check for presence of grates and obstruction of grate tops	Per Batch
Tunnel/ Fermenter drain channels	20 years	Check for obstruction, flush to clear if necessary	Monthly
Tunnel/Fermenter leachate drain valves	5-10 years	Located in manhole to rear of tunnel, check to assure they are unblocked and free running	Weekly
Gas monitoring instrumentation	1-3 years	To be calibrated as required. Check cables for signs of fatigue	Per Batch
Temperature probes	1-3 years	To be calibrated as required by SVS. Check cables for signs of fatigue, and cap for tightness	Per Batch
Tunnel air handling system			
Motors	3-5 years	Listen for bearing rumble, strip and inspect fan blades, grease bearings.	3 months
Motor housing	+10 years		
Pressure sensor	2 years	No maintenance required	
Four way valve solenoid	3 years	Observe solenoid when in operation to assure no slippage is present on the main paddle spindle. Tighten if required	Monthly
Four way valve paddles and housing	20 years	Isolate and remove pipe work to inspect four way valve paddles, also check integrity of seal against lid and valve housing	Monthly
O2 probe	2-3 years	Check for secure fixing of electrical feed and securing nut to main manifold. Calibration of this item can be undertaken by either electrical or manual means. Refer to manual	Monthly
Connecting pipe work	+10 years	Check pipe work for integrity and fit, tighten or change out pipe fixings if required.	Weekly
Fittings	3-4 years	Check integrity	Monthly
Recirculation air valve	10 years	Check handle for signs of fatigue and aperture for free movement of valve doors	Monthly

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Leachate tank			
Leachate tank structure	60 years		
Tank level indicator	3 years	Remove and clean	Monthly
Lift pumps	3 year	Operate frequently to assure pump valves operate freely. Tighten cover fixing screws as required Should pressure be lost, strip down to check for obstruction. Spares readily available. On reassembly, assure valve seats and faces are clean on reassembly	3 months

Compost Equipment			
Orgamix Mixer	7 years	See manufactures specification	
Elevation conveyor	7-10 years	See manufactures specifications	
Menart 1850 Screen	20 years	See manufactures specification	
Loader	5-7 years	See manufactures specification	

Biogas Equipment			
CHP Plant	7 years	See manufactures specification	
Pumps, motors, valves	+5 years	See manufactures specifications	
Connecting pipe work	+10 years	Check pipe work for integrity and fit, tighten or change out pipe fixings if required.	Weekly
Tanks	20 years	Check pipe work connections. Visually inspect for leaks	Weekly
Gas Pipe work	+ 10 years	See manufactures specification	
Biogas Storage Dome	+ 10 years	See manufactures specification	
Solid Separator	+ 10 years	See manufactures specification	

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**Biostabilisation Plant
Operation
CIR20-128**

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Originator

Signed of by

Date Released.....

Purpose

To outline the process for operation of the Biostabilisation Plant

Scope

Biostabilisation Process

Reason For Issue

First Release

Responsibility

Operational Director

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Waste Quantities and European Waste Codes (EWC)

The proposed development is a combination of wet and dry AD designed to process the following

- 16,000 tonnes of MSW converted to 8,000 tpa of MBT fines (EWC 20 03 01)
- 4,000 tpa of domestic source separated food waste (EWC 20 01 08)
- 3,000 tpa of commercial source separated food waste (EWC 20 01 08)

Overview of Waste Flow

The facility is designed to treat both source separated and mixed waste feed stocks. As such, the incoming feedstock will be either directed to the biological building in the case of source separated material or to the mechanical pre-processing building in the case of MSW. Referring to Figure 3 and Figure 4 the following paragraphs will explain the process and waste flow. A more detailed explanation of each step within the process is given in the subsequent sections on dry AD and composting.

The brief mass balance for the MSW and bio-waste inputs to the facility is illustrated in Figures 1 & 2.

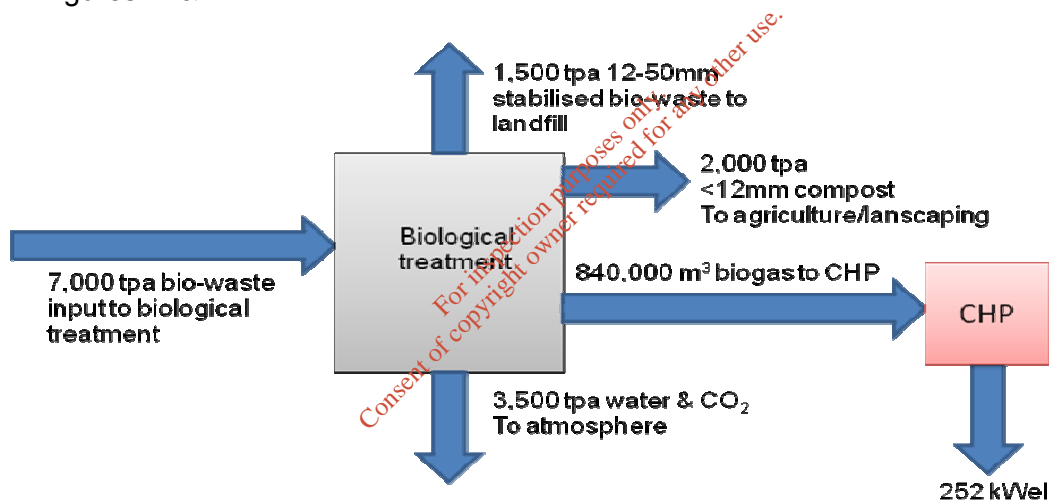


Fig. 1. Mass balance for the bio-waste inputs to the Clean Ireland facility.

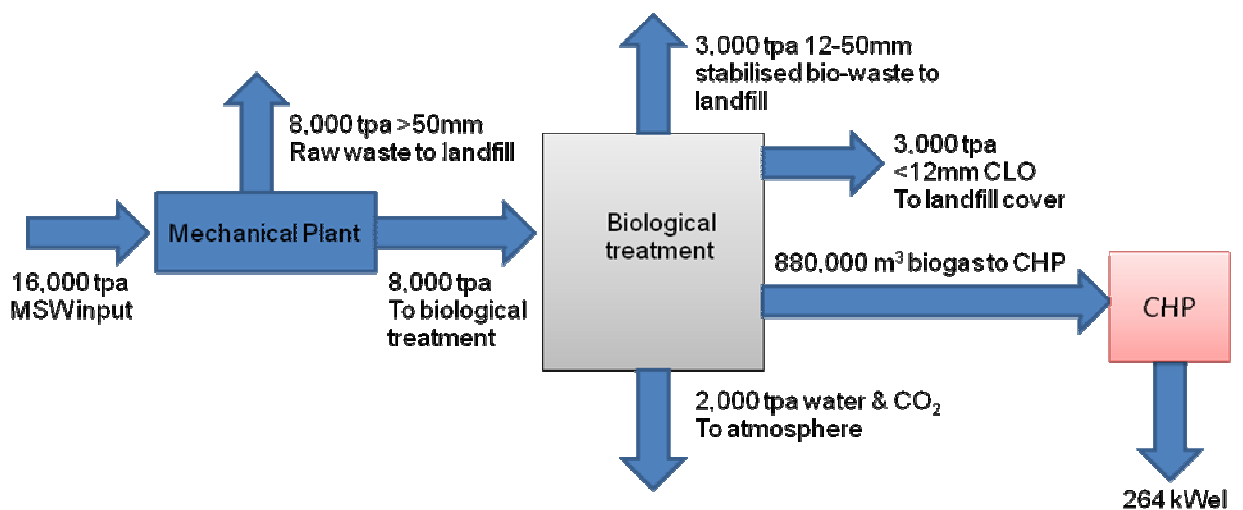


Fig. 2. Mass balance for the MSW inputs to the Clean Ireland facility.

Waste Reception and Pre-Treatment

The reception and pre-treatment of the bio-waste will occur within the waste reception building. The reception and pre-treatment method employed will vary depending on the incoming feedstock.

MBT Fines

The MBT fines consist of organic rich material that is mechanically extracted from mixed waste delivered to the facility. The mixed waste is shredded and screened at 50mm within the MRF section of the facility and the fines (Fig. 3) are conveyed to the biological building by conveyor. These fines are destined for the dry AD processing stream and will be delivered to the facility in a form that will not require any further pre-processing. The MBT fines will be stockpiled in a dedicated section of the reception building until such time as the volume of feedstock is sufficient to half fill a fermentation chamber (225-325 m³).



Fig. 3. MBT fines currently being produced at the Clean Ireland MRF.

Domestic Co-mingled Food & Green Bio-Waste

The combined domestic food and green bio-waste feedstock will be delivered to the biological facility by refuse lorry in a form directly suitable for dry AD. Consequently, this material is directly tipped onto the reception building floor and then contained within a dedicated reception area (Fig. 4). As was the case with the MBT fines, this material will be stockpiled in the reception area until such time as there is an adequate supply to make a 50-50 mixture with the partially fermented contents of a recently unloaded fermentation chamber.



Fig. 4. Bio-waste being tipped at the Broadpath in-vessel composting facility in Devon (left) and material being held prior to processing (right).

Dry Anaerobic Digestion System

Introduction

Dry digestion is well suited to dealing with stackable bio-waste with lower moisture levels, i.e. >20% total solids (TS). These stackable materials can also have high levels of physical contamination and as a result dry anaerobic digestion is ideally suited to the processing of co-mingled brown bin material and MSW fines. In this system the incoming feedstock is loaded into “garage” like gas tight biocells using a loading shovel with little or no pre-processing required. These biocells are referred to as fermentation chambers. A summary schematic of the dry fermentation process is illustrated in Fig. 5. In brief, bio-waste or MBT fines are loaded into a sealed, gas tight concrete vessel and the anaerobic digestion (AD) process is initiated through the spraying of activated anaerobic percolate onto the biomass. This percolate is kept in circulation through an external percolate storage system. The biomass is heated to 37-40°C and biogas production is facilitated. This biogas is drawn off the tunnels and stored prior to use as fuel in a CHP gas engine.

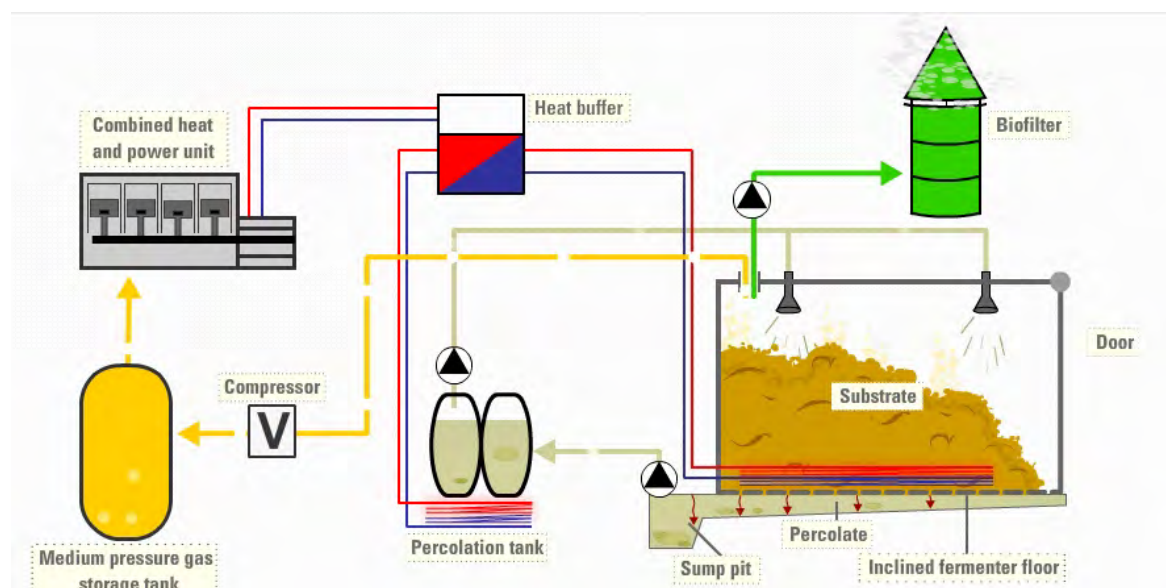


Fig. 5. Schematic of the BIOFERM dry fermentation process.

The system is modular with increasing tonnages of material being managed by additional fermenters. The fermenters are typically 30m long, 7m wide with an internal stacking height of 3.5m. Each fermenter can typically process 2,500 tonnes of bio-waste per year. Due to the cyclical nature of the biogas production process, the minimum number of fermenters is three. This ensures that there is always biogas available to feed the CHP (Fig. 6).

The process of dry fermentation is based on the following procedural steps:

1. Supply and storage of biomass
2. Fermentation
3. Extraction of digestate
4. Ventilation system
5. Gas utilisation

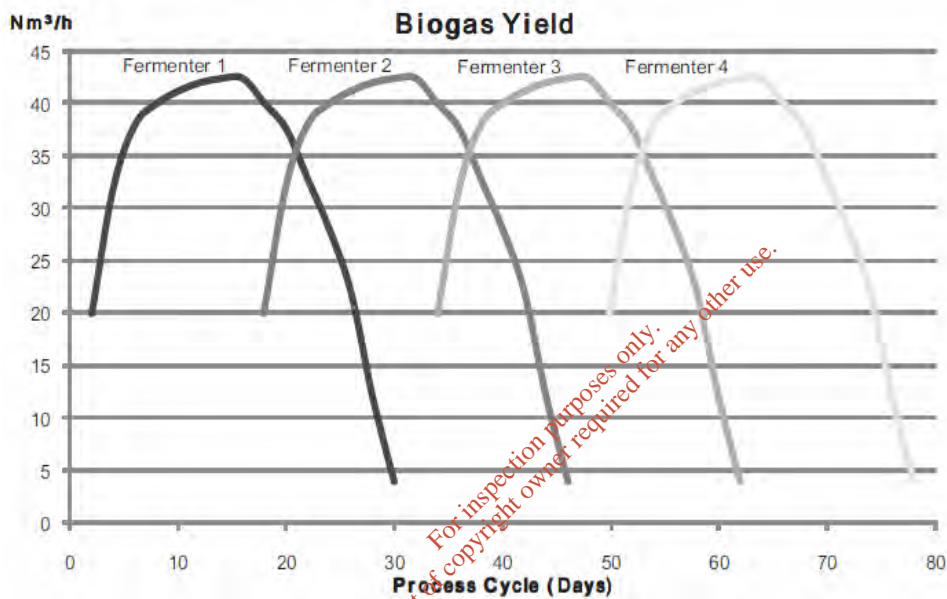


Fig. 6. Typical biogas production cycle from a four fermenter facility.

Supply and Storage of Biomass

When the plant is operational the supply of biomass to the fermentation chamber is based on a 28 day cycle. When a chamber is ready for fresh biomass the first step of the exchange requires the extraction of the partially fermented biomass within the chamber. One portion of the extracted biomass is kept on the building floor and then mixed in an approximate ratio with fresh biomass using a front loader. This ratio will be dictated by the tonnage of material being delivered to the facility and may fluctuate to accommodate seasonal peaks but is expected to be a 50-50 split. The loading and unloading of the solid state digestate is conducted using air-conditioned loading shovels (Fig. 7).



Fig. 7. Filling of a fermentation chamber with Bio-waste.

The Fermentation Chambers

Each of the individual fermentation chamber units has an inner floor area of 7m x 30m with an internal height of 5m (Fig. 8). The height of the stacked biomass however, must not exceed 4.0 meters and this is typically managed at 3.5m. The reinforced concrete fermentation chamber is gas tight to prevent the infiltration of oxygen (the presence of which would cause the methane producing bacteria to become inactive). This also prevents the leakage of biogas to the atmosphere. An in-floor heating system holds the biomass at a constant temperature range of between 37-40°C. The plant engineering components are located in a dedicated technology section housed above the fermenters. The capture and storage of biogas is managed through a stainless steel piped biogas ventilation system while short to medium term gas storage bags are also located above the fermentation chambers. The percolate from the fermenters is stored in two insulated and heated tanks.



Fig. 8. Interior of fermenter prior to filling (left) and with bio-waste prior to fermenter sealing.

To insure that the fermentation chamber is not opened before the methane gas is completely drawn from the chamber and safe atmospheric levels of O₂, CO₂ and H₂S are reached, the air inside the chamber is continuously measured and analysed. The values are communicated to the computerized security system controlling the chamber doors. With the exception of loading and unloading biomass from the

fermentation chambers the entire plant is fully automated by PLC. Interruptions are immediately recognised and documented.

The Percolate Cycle

The dry fermentation process is facilitated by the “percolate cycle”. This involves the spraying of the biomass with an activated anaerobic sludge that is developed in a separate heated tank. This percolate inoculates the biomass while keeping it moist (>70% moisture; <30% solids). While the process of hydrolysis is initiated during storage of the fresh biomass within the reception building, both acidogenesis and methanogenesis steps occur simultaneously within the fermenter. The bathing of the biomass in this activated percolate is key to the process.

In order to drain off excess percolate, a series of stainless steel gutters of 1 m length each with grating are built into the fermentation chamber floor. They absorb excess liquid from percolate sprinkling and route it in a controlled way to a gas tight pipe collection system. From the collection pipes the percolate is routed to the insulated covered transfer pump duct (10 m³) utilising the following equipment:

- Fill level sensor to switch the lift pump
- Transfer pump (mix pump) with pressure pipe to the percolate storage unit
- Ventilated air pipe
- Temperature sensors
- Access door
- Limit Switch

From the transfer pump duct, which is already equipped with a 3-layer coating and a leakage detection system, the fermentation liquid is pressure pumped into an insulated percolate storage unit (Fig. 9). The entire piping system is routed in a frost-proof zone outside the fermentation chamber area. The percolate storage unit consists of the following parts:

- Inlet pipe end
- Filling level sensor to switch the pump
- Transfer pump (mix pump) with pipes to the chamber sprinkling system
- Water tank for excess pressure safety
- Heating (Wall heating)
- Temperature sensor
- Pressure sensor
- Access door
- Limit switch
- Fermentation chamber connection unit

This percolate storage unit is installed with capacity to hold enough percolate for the entire fermentation process (even in the case of dry or highly structured material) where excess water may need to be added. The percolate storage unit is heated via a heat exchanger attached to the CHP unit. A temperature meter is located in the storage unit and takes real time percolate temperature measurements. By doing this, the heat circulation pump can be controlled and when necessary turned on/off.

The percolate is pumped to the individual fermentation chambers via HDPE pressure pipes. The percolate pipes route to the sprinkling unit of the fermentation chambers through gas tight ceiling ducts. A time sensitive control system determines the

maximum percolate sprinkling requirement of the biomass. The cycle comes to an end when the percolate has seeped through the biomass. The remaining bacterial fluid is collected, siphoned and then transported using the transfer pump duct. This is to ensure that the percolate cannot leave the system in an uncontrolled manner. Should the gauge in the percolator storage unit fall below the minimum level required for fermentation of exceptionally dry biomass, fresh water can be applied to the biomass. As a general rule the percolate level should be balanced as the percolate is recycled and stored in the final storage chamber.



Fig. 9. Percolate storage at a Bioferm facility in Japan.

Heating

Less than 5% of the heat generated from the CHP engine is utilised to maintain the working temperature within the fermenters; the rest can be used for external purposes. The thermal energy from the CHP engine is passed to a heat-exchanging device whose operating temperature averages around 85°C. By means of heat pumps, warm water is channeled through the heating system of the biogas plant. The fermentation system is conducted at mesophilic temperatures of around 37-40° C. Heat is transported through stainless steel pipes. The fermentation chamber floor is equipped with heat piping so that the temperature of the fermenting material is maintained at 37-40° C. The placement of the heat distributor alongside the heat in-feed of the percolate storage units ensures against excess heat exchanges.

Pneumatic Controls

The compressor produces the required compressed air to activate all pneumatic valves and it is regulated with an on/off switch. The air pressure lines are routed to a

distribution manifold to facilitate individual valve requirements. In the case of pressure loss or a controlled emergency stop, all pneumatic valves are depressurised automatically through a closing mechanism, using the spring-break principle, thus securing the plant in a safe operating state and preventing uncontrolled gas leaks. Pneumatic valves are activated by the air pressure from the respective chambers: The chamber door is manually opened and closed. When the door is closed, it is pneumatically locked. Compression couplings generate the necessary surface pressure and use it to assure the chamber remains gas tight. In order to open the fermentation chamber door, clamping screws require loosening and a pneumatic release device needs to be operated by hand. Only when gas quantities of $\leq 3\%$ CH₄, $< 0.5\%$ CO₂ and $> 18\%$ O₂ are measured in the fermentation chamber is approval to open the door given via the PLC system (green indicator on control panel). The pneumatic lock on the chamber door can then only be opened with a key. There is a finite time limit within which the chamber door must be opened. If the door is not opened during the allowed time a new approval sequence must be given by the PLC control system based on the content of methane and oxygen in the fermentation chamber.

Gas Measurement and Storage

After loading the fermentation chambers, the biomass is kept undisturbed for a period of approximately four weeks, during which time the biomass is anaerobically fermented and biogas is produced. The gas quality (CH₄, CO₂, H₂S and O₂) is determined with a gas analysis device and communicated to the PLC system and the Siemens SCADA software interface (Figs. 10 & 11). The plant operating parameters such as temperature, pressure, gas quantity and quality are stored in a database. Percolate quantity, valve and plant conditions (fermentation chamber, gas storage, CHP) are monitored via the PLC.

The biogas is extracted from the chamber with an explosion and leak proof ventilation mechanism and it is routed into the gas storage unit located on top of the fermentation chambers (Fig. 12). The internal pressure of the gas storage unit under normal operating conditions is maintained at a maximum of 5 mbar. For safety reasons the internal pressure of the gas storage unit must never exceed 25 mbar. This is controlled by the PLC with a further mechanical pressure relief valve that routes the excess biogas to a flare. The gas storage bag is designed with enough capacity to buffer the biogas even during offline maintenance works on the degasification units of the plant or the CHP unit. When the degasification unit or the CHP unit comes back online the buffered gas can be reprocessed. Under normal operation the gas storage units are loaded to a maximal of 30 - 40 % of capacity via the level control sensor to guarantee enough buffer capacity for operational disturbances.

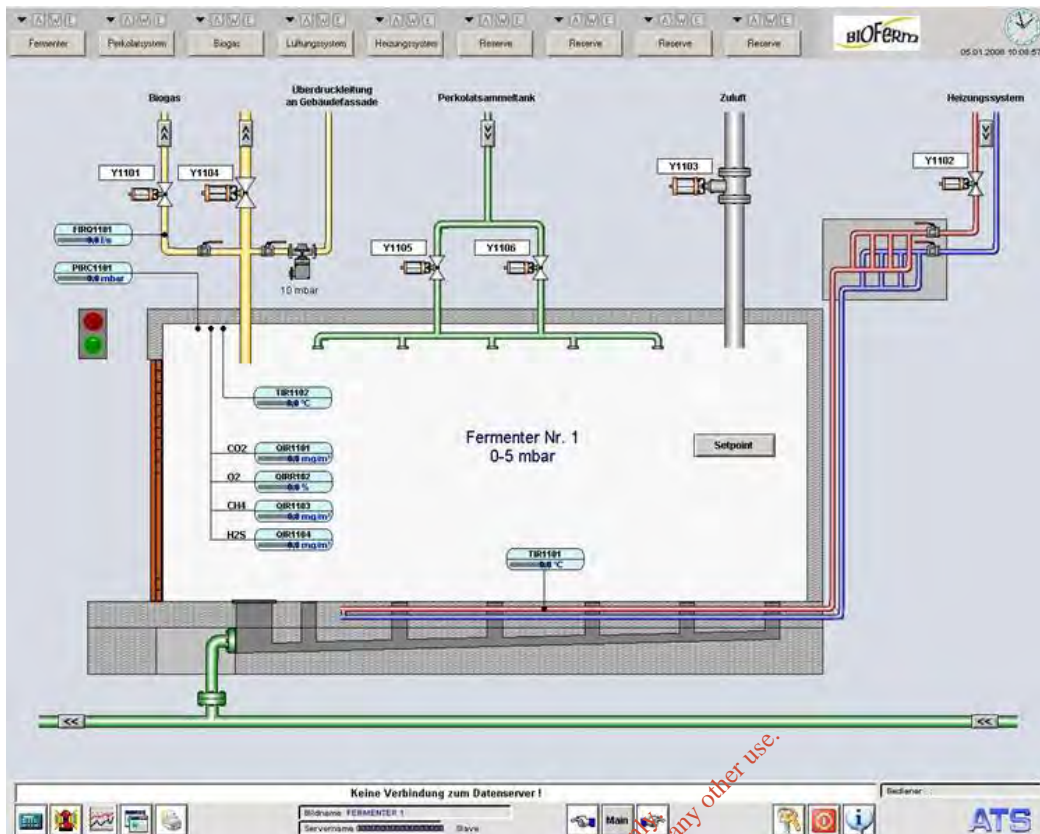


Fig. 10. Siemens SCADA control of fermenter No.1 at the Moosdorf facility in Bavaria.

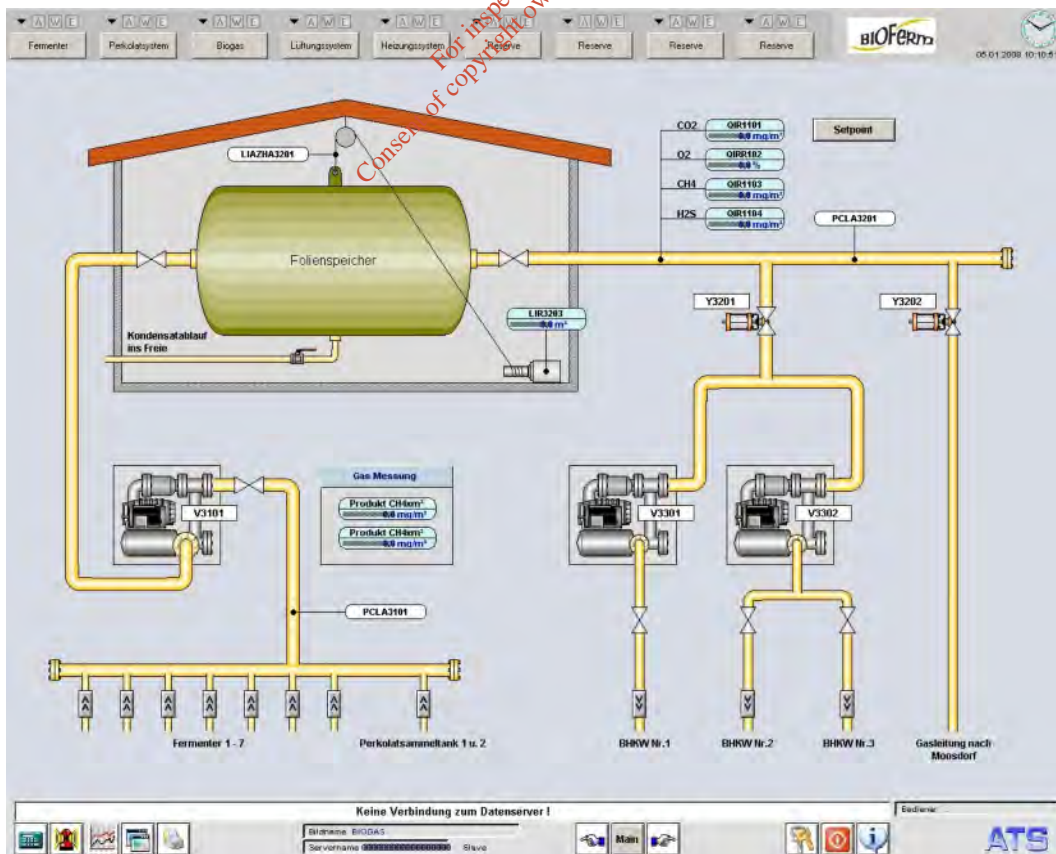


Fig. 11. Siemens SCADA control of gas storage at the Moosdorf facility in Bavaria.

By mixing the streams of gas from different fermentation chambers a gas with consistent methane content is produced. Due to this process the methane content of the mixed gas will be the average of the combined fermentation chambers thus achieving higher process stability. A minimum mixed gas methane content of 57% is aspired to. The desulphurisation of the gas is achieved automatically by the PLC control system. A hydrogen sulfide level of less than ≤ 100 ppm is desired. The moist biogas stays in the gas storage unit for a period of time while cooling to ambient temperature. During this process the water in the gas condenses and is transferred via a siphon water duct (150 mm) from the deepest point of the gas storage unit to the fermentation chamber below. This process is referred to as passive condensation extraction. Further biogas production takes place in the percolate storage tank. A connection to a fermentation chamber is installed on the ceiling of the percolate storage tank and the biogas is exhausted via a gas compressor. The gas is condensed and routed to the gas storage unit.

Continuous measurement of CH₄, CO₂, H₂S and O₂ levels and gas volume for each individual fermentation chamber as well as the volume and composition of the mixed gas in the gas storage unit is carried out to monitor the line operation. This is essential for optimal control of all processes and any interruptions can be detected and prevented at an early stage.



Fig. 12. The pneumatic gas collection system on the roof of the fermenters (left) and the gas transfer blower to the gas bag located in the roof space above the fermenters (right).

A fermentation chamber gas extraction unit consisting of the following components is attached to each fermentation chamber on a gas tight ceiling conduit:

- Valve to the CHP
- Valve for the gas collection pipes with gas meter.
- Hydraulic safety valve for vacuum and pressure gauge

Fermenter Ventilation System

The ventilation system provides sufficient ventilation for the fermenter chamber opening process. Ventilation is accomplished with a controlled piping system (stainless steel, resistant to methane gas and electrical conductivity), backpressure valves and ventilation units. The exhaust air within the fermentation chamber is combined with compost exhaust and the building air which is ultimately discharged to the atmosphere via a bio-filter.

CHP

The CHP unit is supplied with biogas from the respective gas storage units via an individual gas control valve and gas compressor. The CHP units are installed in a separate, noise dampened containerised unit (Fig. 13). The electricity produced by the CHP units is fed into the public grid and/or used for internal consumption. The thermal energy generated by the CHP units is needed in small amounts as process heat (approx. 5 %) in the plant (in-floor heating of dry fermentation chambers, heating of buildings etc.); the surplus thermal energy can be provided for external thermal use. In cases where the thermal energy is not used, the CHPs are equipped with a standard emergency cooling mechanism.



Fig. 13. Containerised CHP at the Decker biogas plant in Northern Germany

The accessories to the gas engines include the compressors, fire and smoke detectors within the room, a separate electrical control cabinet and remote control that enable the supplier to check the biogas engines on a daily basis or according to requirements. Exhaust gas emissions will be in accordance with European standards. Details can be adjusted for local requirements. Noise and exhaust gas quality are based on European regulations. All the safety design is according to German Safety Regulations for Agricultural Biogas Plants. In a situation where the gas engines are out of operation due to maintenance or repair, an emergency flare burns the surplus biogas. The emergency flare has a fully covered flame and is automatically turned on by the level control of the gas holder. It burns biogas at about 800 – 850 °C and follows international standards for this duty.

In-Vessel Composting System

The Compost Tunnels

Three aerobic tunnels are provided (30m x 7m x 5m) to post process the dry AD fermenter output for both the MBT and source separated outputs from dry fermentation. The tunnels are constructed from re-enforced concrete designed to withstand strong chemical attack and high abrasion (Fig. 14). They are sealed by insulated stainless steel lined sliding doors. The tunnels are equipped with a proprietary “C:N” aerated floor system with a computer controlled blower system that is mounted in a gallery on the roof of the tunnels overlooking the tunnel loading area. Approximately 50% of the output from the fermenters is transferred to the aerobic composting tunnels on each cycle and the material is mixed with screen overs to inoculate the material with aerobes.

This material is then stacked within the composting tunnels and aerated. The material readily de-waters and the aerobic microbial population rapidly increases. This is reflected by the auto-thermic increase in temperature of the biomass into the thermophilic range.



Fig. 14. Exterior of the composting biocells illustrating the sliding doors (left) and the proprietary C:N in-pavement aeration system (right).

Control of the Composting Process

The composting process for the tunnels is controlled by a PLC / PC interface, which dictates the airflow within the biomass. The flow of air responds to temperature, pressure and oxygen changes in the composting mass that are continuously recorded by the PLC.

At the beginning of the process, when the composting mass is heating up, the computer system is in “oxygenation” mode. Here the process control system is programmed to blow air into the vessels on a periodic basis to maintain adequate oxygen levels and stimulate the growth of aerobic bacteria. A diagram of the aeration system is illustrated below. The blower system is illustrated in Fig. 16.

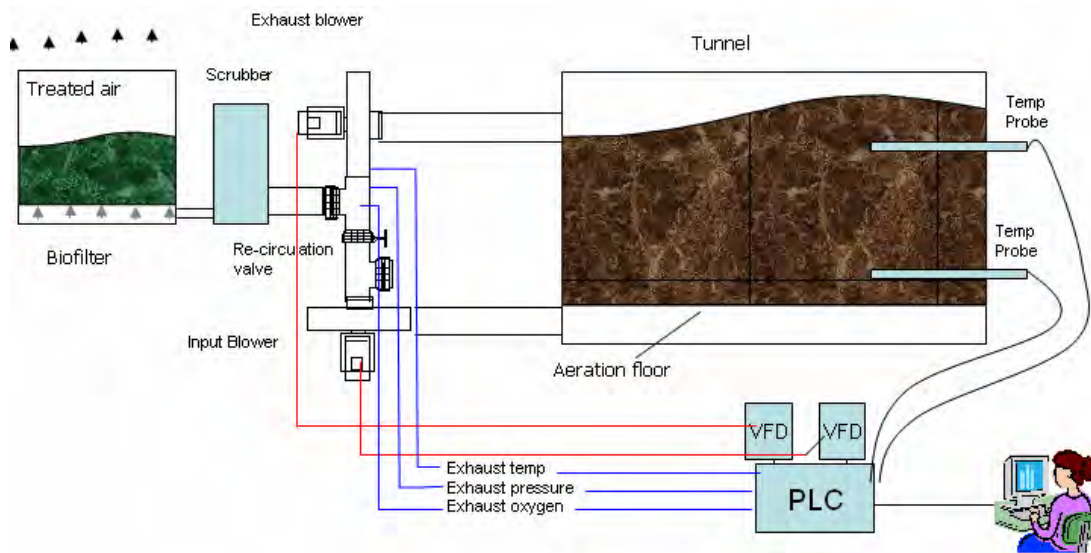


Fig. 15. Schematic of the CCS PLC controlled biocell aeration system.

The PLC coupled with a windows based PC computer allows the operator to configure a temperature profile for the 14-28 days of post fermentation composting and bio-drying. This allows the temperature within the biomass to be controlled within set limits while excess moisture is driven off. Typically the compost would be turned within 7-10 days to break up compaction during this aerobic stage. At the end of this period, a compost at Rottgrade IV will be produced with a moisture content of 35-40% that is then retrieved from the composting tunnels for screening.



Fig. 16. The blower modules in the gallery of the Deepmoor tunnel composting facility in Devon.

Compost Screening

The screening plant is housed within the building to ensure that there are no fugitive emissions of odorous air during the screening operation (Fig. 17). In order to achieve ABPR compliance, both MBT and source separated materials will be screened at 12mm. The overs from the MBT line will be landfilled as stabilised bio-waste, while a proportion of the source separated overs will be used to inoculate the digestate prior to tunnel composting. The unders from the 12mm screen will be segregated for pasteurisation.



Fig. 17. Housed trommel screen illustrating multiple sections that produce different grades of compost and overs.

Compost Pasteurisation and Storage

The trommel screen will produce a fine grain 12mm compost fraction from both MBT and source separated lines. This material will be loaded into a dedicated pasteurisation tunnel that is aerated under maximum re-circulation. Recently screened compost will generate a short period of increased microbial activity due to the physical abrasion resulting from screening. As a result, this compost will reach high temperatures (60-80°C) in the following days if oxygen is supplied. This is facilitated within the controlled tunnel environment and while temperatures in excess of 70°C can be expected in the following 48 hours, additional heat can be introduced from the CHP heat exchanger that is connected to the input blower as a fail safe feature.

After the pasteurisation set points have been achieved, the blowers automatically revert to heat exchange mode to bring the temperature down and thus facilitate further mesophilic maturation during the remaining 4-7 days. This also ensures that when the compost is retrieved from the back door of the pasteurisation tunnels odour is all but eliminated.

An area at the back of the facility has been designated for compost storage prior to release off site. The area will allow for approximately 2-3 weeks of compost storage to allow quarantine and seasonal demand issues (Fig. 18).



Fig. 18. Compost storage at the Waterford city Compost facility.

ABPR Compliance

The Animal By-Product Regulation (ABPR) was introduced into European legislation in 2002 on the back of concerns over exotic animal diseases such as foot and mouth and BSE. Regulation (EC) No. 1774/2002 of the European Parliament and of the Council of 3 October 2002 lays down health rules concerning animal by-products not intended for human consumption. This regulation defines animal by-products as *“entire bodies or parts of animals or products of animal origin... not intended for human consumption”*. A distinction is drawn between the measures to be implemented in the use and disposal of the material concerned, depending on the nature of animal by-products involved.

Under the Regulation

- A composting plant is defined as *“a plant in which biological degradation of products of animal origin is undertaken under aerobic conditions”* and
- A biogas plant is defined as *“a plant in which biological degradation of products of animal origin is undertaken under anaerobic conditions for the production and collection of biogas”*.

Article 15 of Regulation (EC) No. 1774/2002 requires that biogas plants and composting plants shall be subject to veterinary approval by the competent authority. Under Article 6 of S.I. 248 of 2003, the European Communities (Animal by-products) Regulations 2003 which implements the above Regulation, the Minister at the Department of Agriculture, Fisheries and Food (DAFF) may grant an approval, attach conditions to an approval, revoke or vary a condition, withdraw an approval or refuse an application.

As described in Section 1.8, the option of processing the compost at the back end in accordance with EU 1774 is being pursued. In this configuration, the incoming bio-waste is managed in the fermenters and biocells in accordance with best composting and fermentation practice. At the end of this process and as described, the material is screened @ 12mm and this fine grade material is placed in flow through tunnels that facilitate the attainment of the 70°C protocol with the aid of external heat from the CHP as required. This latter heat re-use option is a distinct advantage of the fermentation/composting configuration. The other advantage of this approach is that former foodstuffs can also be processed thus maximizing the band width of bio-wastes that can be accepted by the facility.

Other aspects of the ABPR that the facility design has addressed include the full enclosure of the building and process with stock-proof fencing around the full waste management facility. In addition, all personnel access doors will be fitted with foot baths.

In accordance with the requirements of the latest guidance document published by DAFF, Clean Ireland will undertake the process of phase 1 and 2 ABPR application based on this facility configuration including the development of the facility HACCP plan in parallel with the facility operators manual and SOPs. Once material is available for pasteurisation, there will be a requirement for the facility to pasteurise six concurrent batches and to produce temperature and pathogen data as part of the final license confirmation process. Specifically, Clean Ireland will expect the facility to achieve validation when six batches have been demonstrated to have achieved the time/temperature requirements of the ABPR and to have passed the *E.coli* and Salmonella testing requirements. This is expected to take approximately six months from the date of reception of the first waste loads.

Celtic Composting Systems have been retained to achieve the ABPR license for the facility having successfully delivered on licenses for Galway City Council, Waddock Composting and Waterford City Council compost facilities in addition to a range of facilities in the UK.

COMPOST QUALITY

COMPOST QUALITY (SOURCE SEPARATED MATERIALS)

A good compost quality is clearly a key requirement of this facility. Compost quality parameters can be broken down in a number of key categories:

- (a) Maturity / stability
- (b) Microbial sanitization
- (c) Trace metal concentrations
- (d) Nutrient content
- (e) Level of physical contamination

Maturity

In relation to maturity, it is expected that the proposed Irish compost stability standard of 13mmolO₂/gVS/h will be achieved (Prasad & Foster, 2009). Typically, the source separated bio-waste will be subjected to approximately eight weeks of dry fermentation followed by three weeks of post composting giving a total retention time of 11 weeks. This retention time within a managed biological treatment system will ensure that the requisite level of maturity is achieved (Fig. 20).

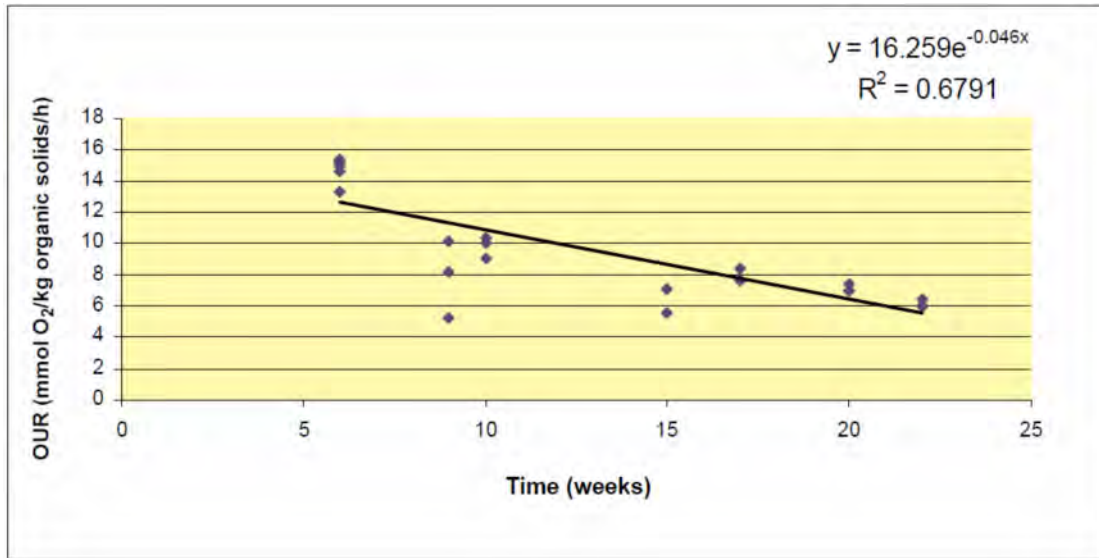


Fig. 19. Oxygen Uptake Rate (OUR) for compost against retention time (Prasad & Foster 2009).

Microbial Sanitation

This is specifically dealt with in accordance with DAFF Animal By-Products Legislation in relation to Salmonella and *E. coli* levels in the output compost product. The regulations state "Sampling must be carried out on digestive residue during or immediately after processing (i.e. immediately after processing parameters have been achieved) in the case of E.Coli, and during or on withdrawal from storage for Salmonella".

Under the regulations the plant must comply with the following standards

Escherichia coli: n = 5, c = 1, m = 1000cfu, M = 5000cfu in 1 g;

or

Enterococaceae: n = 5, c = 1, m = 1000cfu, M = 5000cfu in 1 g;

and

Representative samples of the digestion residues taken during or on withdrawal from storage at the plant must comply with the following standards:

Salmonella: absence in 25 g: n = 5; c = 0; m = 0cfu M = 0cfu;

where:

n = number of samples to be tested;

m = threshold value for the number of bacteria; the result is considered satisfactory if the number of bacteria in all samples does not exceed m;

M = maximum value for the number of bacteria; the result is considered unsatisfactory if the number of bacteria in one or more samples is M or more; and

c = number of samples the bacterial count of which may be between m and M, the sample still being considered acceptable if the bacterial count of the other samples is m or less.

Trace metals

The concentration of trace metals in the final compost from facilities processing source separated bio-waste is directly linked with the concentration in the incoming material and a high correlation has been found between the level of physical contamination in the incoming bio-waste and the final compost. As a result, the control of this parameter is primarily the responsibility of the collector who is in a position to police the quality of the source separation schemes. In addition, it has been found that high levels of overs re-use containing plastics and metals has a detrimental effect on compost metal concentrations. As a result it is imperative that the >50mm fraction is removed from the process at every pass to avoid this material that contains much of the contamination from being re-processed. PVC has been identified as a particular problem in this regard. Facilities that have failed to do this tend to experience a noticeable increase in lead and zinc concentrations with subsequent issues as regards use of the final compost product.

Nutrient Content

While no standard has been set for these parameters, the data attached in Appendix 2 is for information. CCS uses the nitrate / ammonium ratio as a guide to maturity and process stability.

Physical Contamination

Similar to trace metals, physical contamination is a function of the quality of the incoming bio-waste. However, as the facility will not be using high speed shredders and will be screening the final product @ 12mm, this will preclude much of these contaminants, i.e. film and hard plastics, metals and textiles etc. The data attached illustrates that low levels of physical contaminants are possible as a result even from relatively contaminated bio-waste streams as has been experienced at the Waterford City and Galway City facilities.

COMPOST QUALITY (STABILISED BIO-WASTE)

The principal issue regarding the compost quality derived from mixed waste inputs is the stability of the output. Specifically, MBT is a process that is designed to biologically stabilise waste prior to landfill. Such stabilised wastes will have a substantially lower potential to generate landfill gas with resultant significant reductions in greenhouse gas emissions. In addition, the leachate strength from such material will be considerably lower than in the case of raw waste. In Ireland, the EPA has published a standard for stability:

'stabilisation' means the reduction of the decomposition properties of bio-waste to such an extent that offensive odours are minimised and that either the Respiration Activity after four days (AT4) is below 10mg O₂/g dm or the Dynamic Respiration Index is below 1,000 mg O₂/kg VS/h.

This standard must be met for qualifying waste in 2010 and is to be increased to **7mg O₂/g dm** by 2016 in accordance with the requirements of the EU Landfill Directive. The Clean Ireland facility is designed to achieve the 2016 standard given the design life expectancy of the facility (20 years). This increase in stabilisation as a result of the combined anaerobic and aerobic processing is illustrated in Fig. 21 below. The threshold illustrated is **5mg O₂/g dm** based on German standards. Given a design combined retention time of nine weeks, the Irish 2016 standard will be readily achieved.

The facility will produce two bio-stabilised products from the MSW stream. The first will be a 12-50mm material that will have been subjected to the full nine weeks of

biological processing. This material will be destined for the landfill void as stabilised bio-waste in accordance with the EPA stability standards or will be thermally treated as a refuse derived fuel (RDF). The other product consisting of pasteurised <12mm compost will be used as a landfill cover. This material will not be used in agriculture, landscaping or horticulture due to the mixed waste nature of the origin material. The stability of this material will be the same as the coarse fraction. However, due to the fine grain nature of the material, the level of physical contamination is expected to be less than 3% by weight thus making it suitable for use as a cover material. Clean Ireland will also investigate alternative uses for this material for bio-remediation purposes in accordance with EPA guidance.

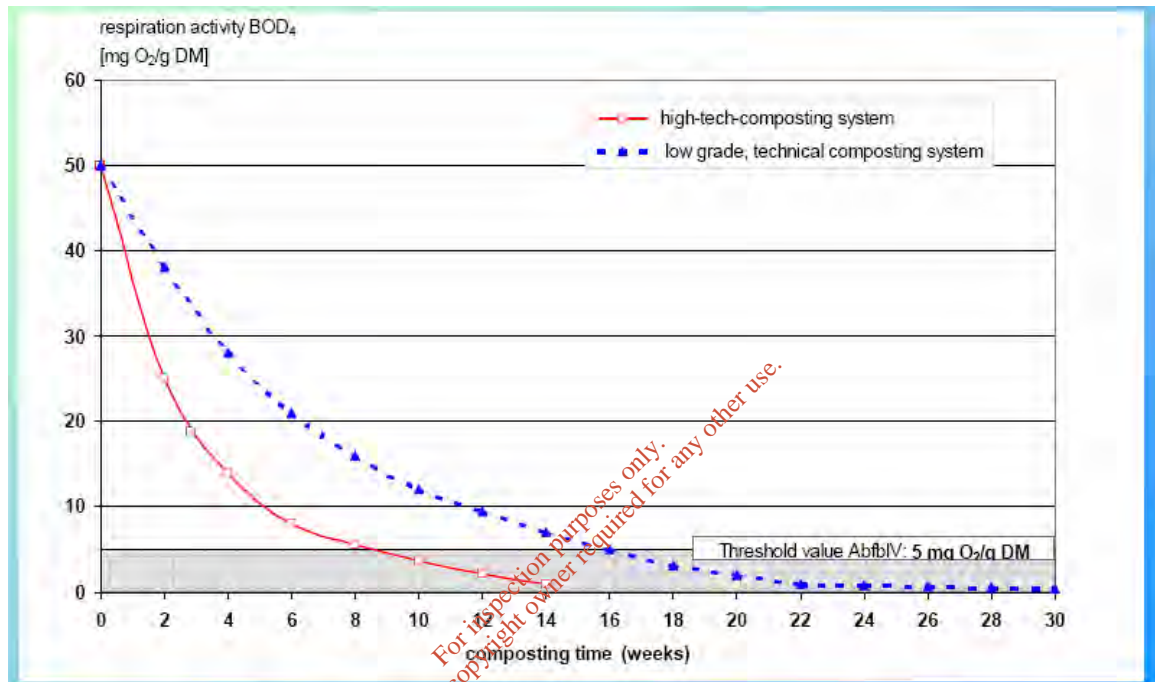


Fig. 20. Reduction in the AT₄ value of mixed waste comparing in-vessel composting and windrow composting techniques.