

## 10.1 Introduction

This chapter of the Environmental Impact Statement (EIS) provides a description of the existing hydrology and surface water regime in the vicinity of the proposed development site at Pass of Kilbride, County Westmeath. The surface water section establishes baseline conditions in the area, in terms of flood risk, general site drainage and surface water quality.

Additionally this chapter will assess the potential impact of the proposed development on the surrounding surface water environment.

## 10.2 Study Methodology

A desktop study was undertaken in January and February 2004 to obtain and examine existing surface water data in order to predict potential impacts of the proposed development on the surrounding environment. The desktop study was supplemented by site-specific investigations. This information was used to establish the baseline conditions in respect of water quality, general site drainage and flood risk assessment. An assessment was made of the unmitigated impact that the development could have on the local environment. Following on from this a number of mitigation measures were introduced to maintain and / or improve the current hydrology and drainage status of the proposed site and local area.

The approach outlined above included design calculations for potential surface water management features for the final site development profile, including flood balancing and sedimentation ponds. All relevant calculations are included in Appendix 10.1.

## 10.3 Desktop Study

The desktop study comprised a review of existing published data pertaining to the general area around the site of the proposed development area. The main sources of information for the study were:

- Met Éireann meteorological data, in particular rainfall and evapotranspiration data;
- EPA Parameters of Water Quality - Interpretation and Standards 2001;
- EPA (interactive) River Quality Map (<http://www.epa.ie/rivermap/data/N13.html>);
- Consultations with the Eastern Regional Fisheries board.

The main findings of the desktop study are described in subsection 10.5 below.

## 10.4 Site Investigation

A site investigation was carried on the 10/12/03 by Enviros staff in order to identify the location of all surface water drains, ditches and streams in the vicinity of the proposed development area. The main features identified during this investigation are shown on Figure 10.1.

A total number of seven surface water samples were taken (SW6 and SW4A (Figure 10.1). Water samples were taken on 10/12/03. Details of sampling procedure are given in the Sampling Procedure. All samples were analysed for a range of parameters.

A second set of water samples were taken downstream of the site and referenced to confirm previously recorded results.

A list of baseline parameters was examined in accordance with the EPA Application guidelines. All surface water regime is in accordance with National Regulations SI No. 439 of 2000 and National Regulations, SI No. 294 of 1989.

Flow measurements of the stream were taken at the site and in the area.

The results of the site investigation are discussed in the following section.

## 10.5 Receiving Environment

### 10.5.1 Surface Water Features

The site is located in Co. Westmeath appropriate to the surrounding area. The land is characterised by extensive peat bog cover to the west and south.

There are a number of watercourses in the vicinity of the site. The watercourses to the northwest of the site comprise a network of small ditches that interconnect to form a main drain. This main drain is a tributary of the Kinnead River at the northern boundary of the proposed site. A ditch runs along the eastern boundary. This ditch also discharges into the Kinnead River.

The proposed site is bound to the north by a peat bog. The peat extraction are evident to the west, while a ditch runs along the eastern boundary. The peat reaches depths of up to 4.0m on the site.

Milltownpass Bog is located to the south of the site. It is a peat bog habitat in Europe and one that is becoming increasingly rare. It is a Natural Heritage Area (NHA-site code 000001) and is of great value for future generations.

The eastern portion of the proposed site is covered by up to 1m of peat. This area is soft underfoot and poorly drained, but is part of the field in which arable farming took place. The main portion of the proposed site is covered by a glacial till which is described as a sandy clay or sandy silt.

The peat to the northwest and west and in the east is generally well decomposed and amorphous. Such peat tends to be of low permeability. Till generally exhibits higher permeability than the peat, but the permeability is largely a function of the fines content of the till.

The generally flat terrain, the generally low permeability of the surficial deposits and the large number of deep drainage ditches indicate that this area is naturally poorly drained and is highly susceptible to runoff.

The closest designated watercourse to the proposed development area is the Royal Canal (Natural Heritage Area (NHA): site code N°: 002103), located approximately 5 km to the north of the site. Lough Ennel (pNHA site code N°: 000685, a candidate Special Area of Conservation (SAC site code N°: 000685) and Special Protection Area (SPA site code N°: 004044)) is located approximately 15 km west of the site. The River Boyne is located approximately 17 km east of the site. Other watercourses in the vicinity of the site include:

- Brosna River, a tributary of the Shannon, located approximately 14 km to the west / southwest of the site;
- Riverstown River, a tributary of the Deel (Rahaarney) which flows into the Boyle, located approximately 7 km to the north / northeast of the site;
- Kinnegad River, a tributary of the Boyne, located approximately 1.5 km to the east of the site; and
- Milltownpass River, a tributary of the Castlejordan River which flows into the Boyne, located approximately 2.5 km south of the site.

## 10.6 Surface Water Quality

### 10.6.1 General Area

Biological and physico-chemical river water quality have previously been monitored and recorded by the EPA at a number of locations in the surrounding area. A five point scale of numerical quality values, Q1 to Q5, has been used in Ireland since the 1970s to determine water quality in the absence of chemical data, where Q5 represents unpolluted waters and Q1 represents seriously polluted waters.

The scheme mainly reflects the effects of biodegradable organic wastes on communities of the larger (macro) invertebrate species which inhabit the substrata of all rivers and streams and are pollution sensitive.

Conditions in the vicinity of the site were obtained from the EPA (interactive) River Quality Map (EPA, 2004a). The monitoring location nearest to the proposed site is on the Kinnegad River at a bridge south east of Clonfad House (station number 0060) and has a biological water quality rating of Q3 - Q4 (slightly polluted) (cf. Appendix 10.2). A second monitoring point downstream of this location at station number 0100 has a water quality rating of Q3.

This EPA river quality information provides an indication of anthropogenic influences on the environment by humans and natural changes in the river water quality, establishing baseline conditions of all rivers and streams in the locality.

The Kinnegad River is very important from a fisheries point of view. Recent and ongoing surveys have shown that substantial populations of salmon, brown trout, brook lamprey, crayfish, stone loach and gudgeon inhabit the water body. Under Annex II of the European Habitats Directive (92/43/EEC) species such as salmon, brook lamprey and crayfish are listed as protected species. The Kinnegad River is also an important salmonid nursery with extensive spawning evident in the upper reaches (N. McGloin, Eastern Regional Fisheries Board, April 2004).

### 10.6.2 Proposed Site

In addition to the general water quality assessment on the 10/12/03 to assess described in Section 10.4 above. Monitoring sheets are provided in Appendix 10.4.

The test results were compared with the limits for human consumption. Water quality with potassium and sodium levels were observed during both sampling rounds. Metals at satisfactory limits at all surface water at acceptable limits throughout the assessment.

A slight increase in chemical oxygen demand (SW1, SW2 and SW3) between December recorded at SW5 and SW6 during the initial within satisfactory limits at these monitoring points.

Total organic carbon (TOC) levels were second round of monitoring. Biochemical oxygen demand throughout at all locations and within acceptable limits.

All watercourses were flowing, as observed. Water levels in ditches below ground level 2 and 3 indicated on Figure 10.1 had respectively. The topography of the site is the north of the site to 85.5 in the east.

### 10.6.3 Surface Water Flow

Flow measurements were carried out at the boundary. The results suggest that the flow is approximately 107l/s, while in the drainage dry weather and is not expected to represent.

Run-off calculations were undertaken to estimate in particular to the peak storm flows at the characteristic discharge from the mean annual flood discharge from the site.

The model uses six variables as explanatory factors may be used to estimate the mean annual runoff developed by the UK Institute of Hydrology Stormwater Management Policy for Development the Irish situation more closely than the model.

$$Q_{BAR} = 0.00108 \times AREA^{0.89} \times SAAR^{1.17} \times SOIL$$

where  $Q_{BAR}$  = the mean annual peak flow

AREA = area of the catchment (km<sup>2</sup>)

SAAR = Standard Average Annual Rainfall

SOIL = a term to describe the runoff susceptibility

(cf. Appendix 10.1 for a detailed description).

The SOIL term for the model takes account of the extent of different surface soils which control the infiltration and runoff characteristics of a site. Borehole and trial pit logs from the intrusive site investigation (cf. Chapter 11) were used to evaluate the current condition of the site in terms of permeability and surface runoff susceptibility. The site investigation found that the site was generally overlain by thin peaty topsoil overlying between 1.0m and 3.0m of sandy gravelly clay (till), over sandy gravel. The eastern portion of the site, approximately 9.5ha is covered by up to 1.0m of peat. The derivation of the SOIL value is shown in the Appendix.

The calculations showed that in its current state, the site's peak flow is approximately 109l/s, assuming 9.5ha of peat with low infiltration and 8ha of till with moderate infiltration, and using the Standard Annual Average Rainfall (SAAR) in the locality for 2002 of 841 mm (Met Éireann Data 2003). The equivalent result where the entire site is considered to have low permeability is 134l/s.

The mean annual peak flow from the catchment using the same model was estimated to be approximately 3,060 l/s.

## 10.7 Proposed Surface Water Management System

The facility will comprise approximately 4.8 hectares in area and will be constructed on a concrete pad, designed to collect all surface water runoff from the process and non-process areas. Surface water runoff from the process hardstanding areas will be recirculated into the process to maintain optimum moisture content in the waste. Surplus runoff collected from these areas will be stored in a leachate collection tank and will be treated in the leachate treatment plant, as described in Section 4.8.2, prior to discharge directly into the stream in the north, subject to EPA Emission Limit Values. The leachate collection system is shown in Figure 4.3.

Vehicle washing will be carried out on the return from the waste delivery area. Wash water will be contained in a circulation system at the vehicle wash and will be augmented by a freshwater supply. Mud and silt will be settled out in a separate tank and disposed of to landfill.

The surface water runoff from the paved non-process areas, such as the storage and loading areas and car park, will be collected by grading these areas to gullies which will discharge to the surface water drainage system. The collected runoff will discharge via a silt trap and oil/water separator to the stream that runs along the northern boundary. Runoff from the site access road will be collected by a drain along the road and will discharge to the eastern drain via a silt trap and oil/water separator.

Rain water from roofs will be intercepted by a dedicated roof water collection system. This will be discharged directly to the surface water discharge point, downstream of the silt trap and oil/water separator.

The system will be designed in accordance with relevant standards. Figure 4.4 shows the details of the proposed surface water management system for the facility.

## 10.8 Potential Impacts of the Proposed Development

During all stages of the proposed development (construction, operation and decommissioning/ restoration) the permeability and runoff characteristics of the area and the local topography around the proposed development will be altered. As a result of this there will be an impact on the surface water environment. The effects on the surface water environment are expected to be greatest down gradient of the site. The impacts are described below, followed by measures that can be put in place to mitigate these impacts.

### 10.8.1 Flow Rate Impacts

The facility will be constructed mostly in the area currently underlain by till. Consequently, the nature of surface water runoff conditions will change on the site, as the moderately permeable till is replaced by virtually impermeable concrete.

The runoff calculations for the facility therefore assume that all rainfall falling management system. The control and management system generates large flow volumes, particularly large volumes of water relatively quickly in areas down-gradient of the site, and possibly

### 10.8.2 Water Quality Impacts

The facility will contain substances which site, such as compost leachate, engine solids) etc. The ways in which these could enter the surface water collection system are described below.

#### Leachate

Leachate is the product of any liquid percolating through soluble materials, chemicals and suspended

Inappropriate work practices, such as discharging could give rise to leachate entering the surface water collection system.

#### Fuel Storage

Without procedures to control the management of fuel, significant risks to surface water from spillage

#### Firewater

Contaminated firewater may arise from fire response procedures, firewater may enter features adjacent to the site, carrying pollutants

#### WC Facilities

WC facilities will be provided for on-site use, if not correctly controlled a risk to the

#### Suspended Solids

The proposed activity has the potential to increase sediment during the construction and operation of the facility. During construction, the increased vegetation during construction, the increased erosion could increase the amount of suspended

Spills of green or mixed waste or compost being washed into surface water collection system discharging from the site.

## 10.9 Do-nothing Scenario

Under a do-nothing scenario, there would be no change to the surface water environment in the vicinity of the facility, cutting, pruning and general management

The proposed location would remain unchanged

## 10.10 Mitigation Measures

The following subsections describe measures which will be incorporated into the design and operation of the facility to mitigate against the potential impacts of the development of the site, as outlined above.

### 10.10.1 Flow Rate Impacts

Site measurements suggest that the flow in the stream was approximately 107l/s. This rate was measured during dry weather and is not expected to represent a peak flow for the stream. The mean annual peak flow in the stream is estimated to be approximately 3,000l/s (cf. Section 10.6.3)

The mean annual peak flow from the existing site is estimated as 109l/s, which represents just 3.6% of the mean annual peak flow in the stream.

The assessment of changes in the peak flow rate from the site indicated an increase of between 123l/s and 134l/s, 13% and 23% of the current peak flow from the site, applying the same model used to assess the existing site. This is an increase to between 4.0% and 4.4% of the mean annual peak flow in the stream. These calculations ignored the process water requirements of the facility.

However, the design of surface water collection systems is generally based on a different model referred to as the Rational Method, which tends to give much higher runoff peak flow rates than the FSR models. The Rational Method was applied to the proposed facility to estimate the peak discharge rates from the site for the most intense annual storm, as provided by Met Éireann (6.3mm in 15 minutes for Mullingar). This gave a peak annual discharge of 137l/s. This discharge represents approximately 4.5% of the mean annual peak flow in the stream.

While the annual peak discharge from the development may not represent a large increase in the context of the peak stream flow, more intense storms with longer return periods can be expected during the life of the facility. Higher discharge rates associated with these heavier storms may result in flooding. The surface water run-off from the site will be controlled to restrict flows from the site, thereby reducing the risk of flooding in areas downstream of the site.

This will be achieved by flow balancing, where the discharge flow rate will be restricted by installing a fixed control such as an orifice or vortex flow regulator or by throttling the discharge through a pipe of a specified diameter. These controls will be designed to prevent discharges in excess of the defined peak discharge flow rate, which is proposed to be the pre-development mean annual peak flow of 109l/s.

The surface water discharge will comprise roof water and runoff from non-process hardstanding areas of the facility that has passed through the silt trap and oil/water separator. Flows in excess of peak flow rate will be diverted to a soakaway area between the site and the stream.

The soakaway will provide storage for excess flows and will enable the water to slowly infiltrate through the base of the soakaway to the groundwater table, which provides base flow to the stream in the north. This operation will delay large quantities of water reaching the stream during peak flow conditions.

The soakaway will be defined by small bunds which will contain the runoff. The bunds will be approximately 0.5m high and will provide sufficient capacity to accommodate excess runoff from the 1 in 20 year 1-day storm event, equivalent to approximately 1000m<sup>3</sup>. The area will be planted with trees which form a screen around the site. The soakaway will only receive diverted water intermittently, and as such will not have adverse effects on the trees of the area.

### 10.10.2 Water Quality Impacts

#### Leachate

Contaminated water and leachate will be contained by the concrete base of the facility and collected by means of a series of leachate collection drains, as illustrated in Figure 4.3. The process areas will be graded away from non-process areas to enhance the efficacy of this system. In addition, small ramps will be used to delineate adjacent process and non-process areas, particularly between the ASPs and the storage areas.

This leachate will be collected by a dedicated process areas, and stored prior to recirculation. Leachate will be used to maintain optimum nutrients and micro organisms present in

Not all of the collected leachate will be re-used on a seasonal basis. Quantities of leachate contained prior to treatment in a sequence are shown in Chapter 4. The effluent from the reed bed discharge conditions required by the EPA of the leachate treatment plant is shown in

Cleaning without water, "dry cleaning" will be possible. Where it is necessary to use water, limit contributions to the surface water collection

#### Fuel and Dangerous Substance Storage

The fuel stores will be bunded in accordance with best practice. Bunds are most likely to arise during loading or unloading, that best practice is used for these operations, capacity is maintained for retaining spills.

It is possible for spills and leaks to reach a bund. Fuel oil from cars and site plant and machinery, likelihood of such leaks. All surface water discharging from the site. The silt trap and

All dangerous substances will be stored in accordance with best practice.

#### Firewater Retention

In the event of a fire, firewater will be collected on the area in which the firewater arises. Bunds will contain firewater within those areas.

The leachate collection system will convey water held for testing. The results of the tests will be conveyed to the leachate treatment plant, or whether to

Firewater entering the surface water system will be conveyed to the surface water treatment plant, which will pump water can be pumped from the system to either

Emergency procedures will be developed and implemented on-site.

#### WC Facility

A proprietary treatment system and process specification and location of the treatment system in accordance with the guidelines in the EPA's "Guidelines for Single Houses". The location of the treatment system

#### Suspended Solids

Suspended solids will be removed from runoff by a silt trap to enable

## 10.11 Predicted Impacts

The proposed development will alter the surface water drainage characteristics of the site. The calculations contained in Appendix 10.1 indicate an increase in the mean annual peak flow from the site. Flows in excess of the pre-development mean annual peak flow will be diverted to a soakaway, thereby precluding any significant impact on the flow rates in the stream.

All surface water collected on site will be treated by a silt trap and oil/water separator prior to discharge to the adjacent water bodies. The proposed mitigation measures will minimise the potential impact of leachate, firewater, accidental spills, domestic effluent and surface runoff on the local surface water environment.

It is anticipated that there will be an insignificant impact following the implementation of all the proposed mitigation measures. The operation of the development in accordance with good management practices and the containment provided by the surface water management system will mitigate significant environmental impacts during normal operation.

Accident and emergency response procedures will be prepared for all identified risks, to further mitigate potential impacts.

## 10.12 Monitoring

Ongoing routine surface water monitoring will be undertaken during the operation of the proposed development. All discharges to the surface water environment will be monitored in accordance with the requirements of the Waste Licence.

The surface water silt traps and oil/water separators will be inspected and cleaned on a regular basis. Any material removed from the separators will be disposed of in accordance with National Legislation.

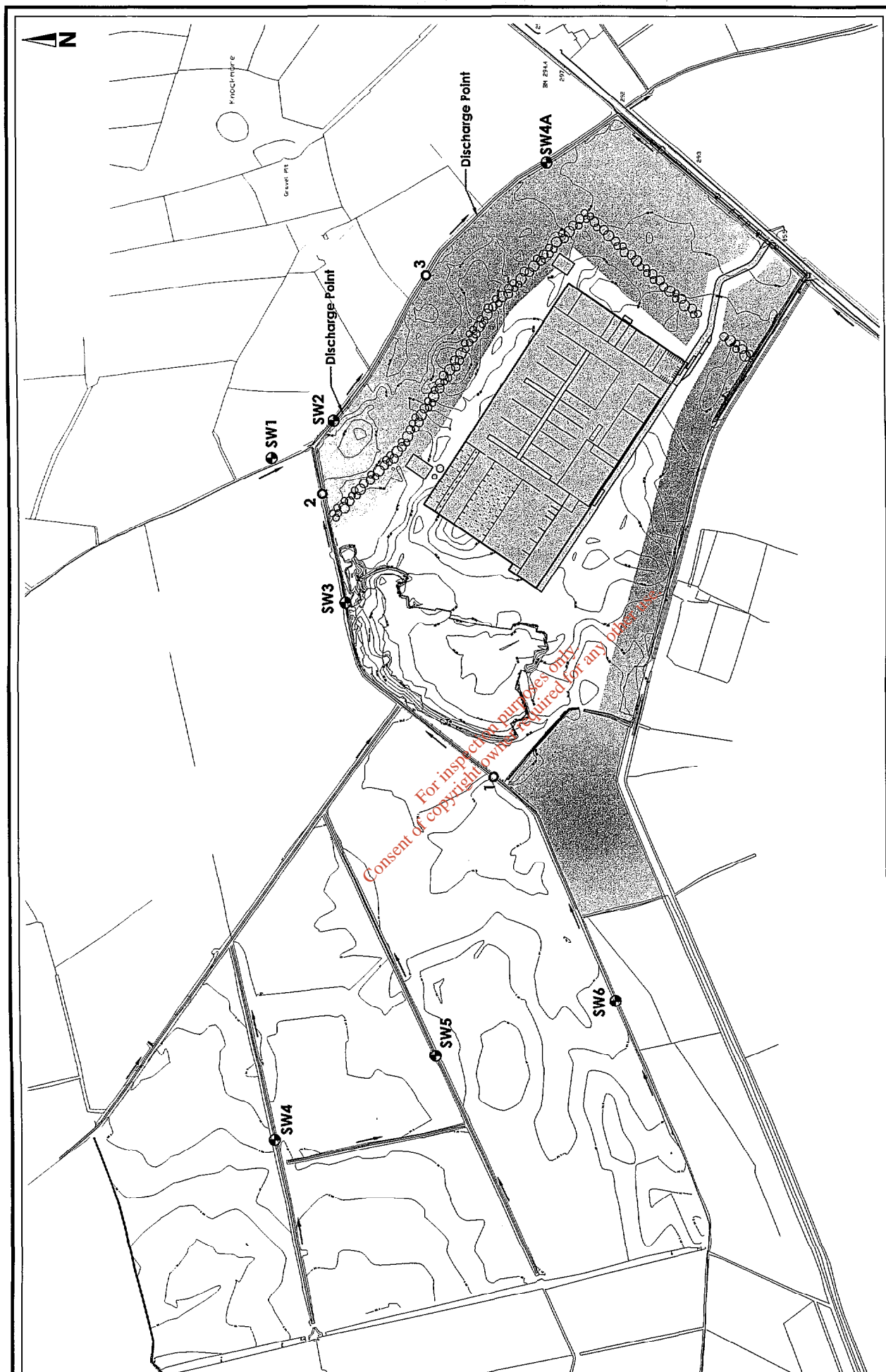
Leachate quality over a range of parameters will also be examined. The final effluent from the reedbed will be monitored for parameters in accordance with the Waste Licence.

## 10.13 Restoration and Residual Impacts

It is anticipated that the proposed facility will operate for the foreseeable future and some restoration details are included in Chapter 4. Should the facility close down, it would be decommissioned as described in Chapter 4. The removal of all wastes, products, fuels and other materials suggests that the source of any risk associated with the site would be removed. Surface water would continue to be monitored until such time that monitoring is not required, as agreed with the EPA.

## 10.14 Conclusion

The design of the facility and best environmental management practices will ensure that the potential impacts of the proposed facility on the surface water environment during operations will not be significant. Should the site be decommissioned and restored, the subsequent impacts on the surface water environment will be insignificant.



KEY:

- Surface water monitoring locations
- Observation point locations
- Flow direction

**FIGURE 10.1**  
SURFACE WATER AND  
MONITORING POINTS