Air Dispersion Modelling Report

Engineered Landfill

Blessington, Co Wicklow

June 2004

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1 Executive Summary

Current Status	The site is located in the county of Wicklow in Ireland and is owned by Roadstone Dublin Limited. The site area is approximately 276 hectares.
Landfill Source	Three unauthorised landfill sites known as Areas 1, 4 and 6, comprising an estimated 50,000 tonnes of domestic, commercial and industrial (DCI) Waste.
Landfill Characteristics	190 x 85m (16,150m ² area) to be capped with a 5mm geosynthetic clay liner overlying a 1mm LLDPE Geomembrane, overlying a 5mm geosynthetic clay liner, overlying a 1m thick clay liner.
Model Parameters	 Singe point emission of vent stack of 3m length and 0.1m diameter. Three potential receptors modelled: 1. Darkers Lane 450m north east from source 2. Residential housing 600m south east from source 3. Site boundary 20m east from source A wind rose with dominant flow direction from the south west was input into the model.
Model Results and Summary	Insignificant risk to human health at all receptors is likely from methane and carbon dioxide. Insignificant risk to human health or potential nuisance at all receptors is likely from odorous trace gas and benzene. Monthly gas monitoring is recommended during the operational phase of the landfill for safety of operators, further information for any remodelling and assessment of the impact of the works on air quality.

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2 Introduction

Over the last few years there has been an increased detection of large scale unauthorised tipping of waste in the county of Wicklow in Ireland. Investigations at the Blessington landholding of Roadstone Dublin Limited (RDL) in early 2003 revealed that approximately 50,000 tonnes of domestic, commercial, and industrial (DCI) waste had been infilled at three unauthorised landfill sites over the last 10 years, together with a similar amount of construction and demolition (C&D) waste. The three unauthorised landfill sites are illustrated as Areas 1, 4 and 6 on the figure reproduced within Appendix A.

Mouchel Parkman has undertaken an environmental risk assessment of the threats to drinking water and groundwater posed by these unauthorised landfills and also reviewed the risks from landfill gas to a recently constructed housing development (Mouchel Parkman, August 2003).

Air dispersion modelling was conducted to predict down-gradient methane and carbon dioxide concentrations as well as potential odour issues that may result from the passive venting of landfill gases from the proposed non-hazardous engineered landfill on Roadstone Dublin's landholding at Blessington.

In addition, benzene was added to the model due to significant levels recorded in Area 6 during the monitoring of volatiles in March 2003. The same levels were also recorded in March 2004 (see Appendix H).

2.1 **Previous Studies**

The Mouchel Parkman Risk Assessment, Report 4000043/OR/03, prepared in consultation with the Environmental Protection Agency, concluded that remediation works of the unauthorised landfills was required due to the risk of landfill gas (recorded within Area 6) to nearby housing under construction. After considering the remediation options in terms of cost, environmental benefits, implementation and public impact, it was decided that all of the DCI waste would be transferred from each of the three affected areas to a proposed engineered landfill to be constructed within the Blessington site (see Appendix A).

It has been calculated that this waste will total approximately 55,000 tonnes of DCI waste. It has been assumed that up to a further 10,000 tonnes of inert C&D waste will also be placed in the landfill during deposition, with the balance of material deposited in the landfill comprising soils beneath and around the buried waste.

The proposed engineered landfill is located approximately 450m from the nearest housing development. These properties located at Darkers Lane are outlined on the figure provided (Appendix A).

2.2 Model Description

The GasSim model version 1.03 (supplied by Golder Associates) was selected for this assessment as it enables the combined contribution of vented gases and those released through the landfill surface cap to be considered. This model assumes that the landfill is a simple point source of emission, with atmospheric dispersion off-site simulated by a Gaussian plume deterministic model.

GasSim is a probabilistic model that uses the Monte Carlo simulation technique to select randomly from a pre-defined range of possible input values (probability density functions – PDF) to create parameters for use in the model calculations. Repeating the process many times gives a range of output values, the distribution of which reflects the uncertainty inherent in the input values. This enables the likelihood of the estimated output levels being achieved to be ascertained.

2.3 Model Assumptions

In modelling the landfill, it was necessary to make various assumptions about the discharge conditions that would then be incorporated into the future engineering designs. The model also required information to be input on the landfill design itself, including the source material composition, deposition rates and hydrogeological parameters. These parameters and their justifications are included in the following sections and are summarised in Appendix B. In general, parameters were chosen to provide a conservative estimation of risk, which is tending to a 'worst case' situation that could apply.

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3 Pollutants and Air Quality Guidance

The following table gives a list of pollutants that were modelled with the relevant environmental assessment levels (EAL's) and odour thresholds. The trace gases were chosen as they form the odorous components of landfill gas; benzene was also chosen as significant levels had been recorded during previous monitoring.

Gas Modelled	Long Term EAL taken from EA's H1 Guidance (mg/m3)	Odour Threshold (mg/m3) - GasSim Default
Carbon disulphide	0.064	0.7
Diethyl disulphide	Not Applicable	0.0003
Dimethyl sulphide	Not Applicable	0.0037
Ethanethiol (ethyl mercaptan)	0.013	0.00046
Hydrogen sulphide	0.14	0.0001
Limonene	Not Applicable	0.02
Methanethiol (methyl mercaptan)	0.01	0.0002
Propanethiol	Not Applicable	0.00014
Toluene	1.91	0.7
Xylene	4.41	0.54
Benzene	0.016	N/A

According to H1 Guidance issued by the EA, air emissions are considered to be insignificant if the maximum process contribution (long term) is less than or equal to 1% of the long term EAL as provided above.

When considering methane (CH4) and carbon dioxide (CO₂), the Irish EPA guidelines of 1% and 0.5% respectively were considered (Irish Department of Environmental Standards for Building Construction).

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[•] UK Environment Agency – Horizontal Guidance Note IPPC H1 "Environmental Assessment and Appraisal of BAT"

4 Landfill Source

For the purposes of modelling we have assumed that source material from Areas 1,4 and 6 will be deposited in the engineered landfill between 2004 and 2005, reaching a total of 65,000 tonnes. This was input to the model as a uniform range of between 19,500 to 23,800 tonnes for 2004, increasing to between 39,000 to 47,700 tonnes in 2005. A zero waste amount was then input to the model for the years between 2006 and 2022.

During the period of waste deposition, it was assumed that 75% of the waste was covered by some form of cap. From the time of completion, in 2005, it was then assumed that all the waste was covered with a capping layer.

For the purposes of the model it was assumed that the 55,000 tonnes of DCI waste was split between approximately equal amounts of commercial, industrial and domestic waste. GasSim contains default waste streams for commonly deposited waste materials filled between 1980 and 2010, from HELGA (Gregory et al., 1999), this is enclosed as Appendix D. The composition of each type of waste was determined for the model using the model default values for 1980's to 2010 waste streams. This was input as a uniform range 21% to 37.4% of total waste input to the proposed landfill for each of the three waste types.

Up to a further 10,000 tonnes of residual C&D waste was also assumed within the model and given as a uniform range between 7.7% and 15.4% of total waste input to the proposed landfill.

Consent

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5 Landfill Characteristics

The landfill area was input as 190m x 85m giving a total area of 16,150 m², which has been assessed as being the potential area of active waste deposited. Biological methane oxidation was limited to 10%, this being the proportion suggested by DEFRA[•] policy.

It is intended that the waste material is to be capped with a 5mm thick Geosynthetic Clay Liner overlying a 1mm thick Linear Low Density Polyethylene (LLDPE) Geomembrane. This was included in the model as a 0.005m thick layer with a hydraulic conductivity of 5E-11m/sec, with a second layer of 0.001m thickness with a hydraulic conductivity of 4.3E-19m/sec. Whilst this may reduce the degree of methane release from the surface it should enhance the content of gases released passively through the proposed landfill gas management system.

It is also proposed that the base of the landfill is to be lined with a 2mm thick high density polythene (HDPE) Geomembrane, overlying a 5mm thick Geosynthetic Clay Liner, overlying a 1m thick clay liner. This was included in the model as a 0.002m thick layer with a hydraulic conductivity of 4.3E 19m/sec, with a second layer of 0.005m with a hydraulic conductivity of 5E tim/sec, and a third layer of 1m with a hydraulic conductivity of 1E-9m/sec.

As the presence of recirculated leachate is likely within the engineered landfill, a 'wet' scenario was selected for the model using the GasSim default.

Previous hydrogeological analysis provided a representative value for the hydraulic conductivity of 0.865m/day (or 0.00001m/sec).

Default values for moderate cellulose decay rates were included in the model set up. It was also assumed that any vented gases would comprise 66% methane in the first instance. 66% methane is the likely maximum concentration of methane in any landfill gas generation (*Department of Environment – Waste Management Paper 27*)

The value for infiltration, uniform PDF of 10 to 15 mm/year (*provided by JBA*), corresponds to 1-1.5% of annual rainfall recorded locally and was decided using professional judgement based on the cap design of the landfill.

[•] DEFRA – UK – Department for Environment Food and Rural Affairs

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6 Emission Parameters - Gas Plant

The GasSim programme has been adapted to model a single point emission. To achieve this, the air / fuel ratio was lowered to 0.01 and ambient air temperature $(20^{\circ}C)$ was assumed, thereby removing aspects of bleeding and heating that would be associated with an engine. Furthermore there was assumed to be no down time to represent constant passive venting. Similarly zero methane destruction efficiency was assumed and no operational flares were modelled. The assumed vent stack dimensions were a diameter of 0.1 m and height of 3 m.

The first model runs were based on emissions occurring from 2004 onwards. The proportion of methane and carbon dioxide in the exhaust streams were input as 66% and 16.8%, respectively, these concentrations having been previously recorded in the landfill (area 6). Predicted levels of generated CH_4 and CO_2 are provided within Appendix E. Production of landfill gas peaks in 2006, with an estimated $87m^3/hr$ of CH_4 and $44m^3/hr$ of CO_2 being generated. With the simulation of a single vent point, generated levels of landfill gas decline to approximately half peak levels over three years. However, generated levels are then shown to gradually decline over the next fifteen years with approximately one eighth of peak levels still being generated in 2024.

Landfill gas generation is expected to occur for approximately thirty years after deposition (*Department of Environment – Waste Management Paper 27*). Therefore predicted levels of landfill gas are expected to continue to decrease after 2024, for approximately 10 more years before the generation of landfill gas ceases. Management measures, such as gas flaring, could potentially be incorporated to reduce the generated levels of methane gas over time.

The model shows that the predicted CH_4 and CO_2 discharge rate between 2004 and 2024 were 6.6m³/hour and 3.3m³/hour, respectively, for a single vent point with the above dimensions. Therefore, at least fourteen separate vents with the above dimensions would be required for dispersion of generated landfill gas at peak levels. The vent output graphs are also attached in Appendix E.

Default concentrations in the landfill gas were assumed for the model and these were compared with trace gas concentrations recorded during monitoring. Particular attention was given to the standard odour suite, which includes a range of sulphur containing hydrocarbons (known as thiols or mercaptans), gaseous sulphides, xylene, toluene and limonene, in addition benzene was added to the trace gas suite. Trace gas default inputs for odorous components of landfill gas are shown in the table (Appendix F), these default trace gas concentrations were derived from performing statistical analysis on the data gathered by a number of authors (AERC draft database, 2001; Derwent et al., 1996; and Stoddart et al., 1999). Concentrations recorded during in-situ monitoring that exceeded the relevant

G:\Inter Divisional\4000043 CRH Blessington\15 Reports & Photographs\Reports\721128-OR- 10 1\Appendices\Appendix 3\4000043-OR-5C.doc © Mouchel Parkman 2005 default values were also input for re-runs of the model, with the outcome discussed in Section 7.

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7 Atmospheric Dispersion Parameters

Dispersion of methane and carbon dioxide to the following receptors was modelled with each receptor assumed to be located down gradient from the venting source to provide the most conservative modelled scenario. The location of the three receptors are shown on the drawing within Appendix A. Each receptor was considered to be at the same elevation as the vent stack, although further analysis (not reported) showed that variation on the height did not influence the results.

Receptor	Distance from Source (m)	Direction from Source
1. Darkers Lane (isolated rural housing)	450	NE
2. Residential Housing (near Area 6)	600	SE
3. Site Boundary	20	E

For air dispersion, a wind rose with dominant flow direction from the southwest was input to the model, *as provided by JBA*. The values input are summarised in the following table:

	Wind Direction	Frequency
	30 net 1	0.03
Con	. 15 CO	0.06
	FOT VID 90	0.10
	120 s	0.05
	¹⁵⁰	0.04
	180	0.07
	210	0.17
	240	0.25
	270	0.13
	300	0.04
	330	0.03
	0	0.03

It was assumed that each receptor was down gradient of the predominant wind direction, thus providing a conservative assessment.

Default values of Pasquill data were assumed. These simulate aspects of atmospheric stability, wind speeds and mixing depths for gases.

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8 Model Results

8.1 Dispersion

Using the GasSim model the predicted atmospheric dispersion of landfill gas to each of the three receptors was modelled as follows.

8.1.1 Bulk Landfill Gas

The predicted methane (CH_4) and carbon dioxide (CO_2) concentrations at the receptors are summarised in the following table. These cover the period from 2005 onwards.

Year	CO ₂ at	CH ₄ at	CO ₂ at	CH₄ at	CO ₂ at	CH ₄ at
	Receptor	Receptor 1	Receptor 2	Receptor 2	Receptor 3	Receptor 3
	1	(mg/m ³)	(mg/m^3)	(mg/m^3)	(mg/m ³)	(mg/m ³)
	(mg/m ³)					
2005	0.0096	0.0054	0.0068	0.0049	0.43	0.23
2006	0.028	0.016	0.017	0.013	1.32	0.72
2007	0.021	0.011	0.013	0.0094	0.95	0.52
2008	0.016	0.0089	0.01	0.0075	0.73	0.40
2009	0.013	0.0074	0.0087	0.0064	0.6	0.36
2010	0.011	0.0063	0.0076	0.0056	0.51	0.28
2011	0.0098	0.0055	0.00680	0.005	0.44	0.24
2012	0.0087	0.0049	0.0062	0.0046	0.39	0.21
2013	0.0078	0.0044	0,0057	0.0042	0.34	0.19
2014	0.0069	0.004	0.0052	0.0038	0.30	0.17
2015	0.0062	0.0036	0.0048	0.0035	0.27	0.15
2016	0.0055	0.00325	0.0044	0.0033	0.24	0.13
		Cor		· · · · · · · · · · · · · · · · · · ·		
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Receptor 1 - Darkers Lane

The model results predict a maximum methane concentration of 0.016mg/m³ at receptor 1, located 450m down gradient from the vent stack, with carbon dioxide reaching a maximum of 0.028mg/m³. In comparison, methane is considered to be toxic by asphyxiation at concentrations in excess of 30% by volume (200,000 mg/m³), a value approximately twelve million times greater than the maximum predicted. Asphyxiation from carbon dioxide can occur at concentrations in excess of 0.5% v/v (9,200 mg/m³), a value approximately three hundred thousand times greater than the maximum recorded.

Receptor 2 – Residential Housing near Area 6

The model results predict a maximum methane concentration of 0.013mg/m³ at receptor 2, located 600m down gradient from the vent stack, with carbon dioxide reaching a maximum of 0.017mg/m³. In comparison, methane is considered to be toxic by asphyxiation at concentrations in excess of 30% by volume (200,000 mg/m³), a value approximately twenty million times greater than the maximum recorded. Asphyxiation from carbon dioxide can occur at concentrations in excess of

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0.5% v/v (9,200 mg/m³), a value approximately five hundred thousand times greater than the maximum recorded.

Therefore, based on the model predictions, the venting of methane and carbon dioxide from the engineered landfill should not pose a risk to public health of occupants in the nearby residential areas. The lower explosive limit for methane is 5% v/v (33333mg/m³). This is approximately two million times greater than the maximum predicted methane concentration (0.016mg/m³ at receptor 1) and hence there is likely to be no significant risk for any explosion at either receptor.

Receptor 3 – Site Boundary

When considering the nearest site boundary, the model predicts a maximum methane concentration of 0.72mg/m^3 at receptor 3, located 20m down gradient from the vent stack, with carbon dioxide reaching a maximum of 1.32mg/m^3 . In comparison, methane is considered to be toxic by asphyxiation at concentrations in excess of 30% by volume (200,000 mg/m³), a value approximately two hundred and fifty thousand times greater than the maximum recorded. Asphyxiation from carbon dioxide can occur at concentrations in excess of 0.5% v/v (9,200 mg/m³), a value approximately seven thousand times greater than the maximum recorded. The lower explosive limit for methane is 5% v/v (33333mg/m³). This is approximately five thousand times greater than predicted methane concentration and hence there is likely to be no significant risk for any explosion at the site boundary.

8.1.2 Odorous Emissions

The emission of landfill gas was also considered in terms of odour thresholds being exceeded at each receptor. The predicted concentrations of trace compounds considered to represent the most odorous emissions from landfills are provided in the tables below, benzene concentrations were also recorded.

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Receptor 1 – Darkers Lane

Predicted Trace Gas Concentrations (mg/m ³) at Receptor 1											
	Carbon Disulphide	Diethyl Disulphide	Dimethyl Sulphide	Ethanethiol	Hydrogen Sulphide	Limonene	Methanethiol	Propanethiol	Toluene	Xylene	Benzene
2005	1.4e-7	9.8e-11	7.6e-7	2.2e-7	1.5e-5	2.6e-6	4.9e-7	9.2e-8	6.9e-6	2.3e-5	4.3e-9
2006	4.3e-7	9.5e-11	2.3e-6	8.0e-7	4.1e-5	7.6e-6	1.4e-6	2.6e-7	2.2e-5	6.6e-5	1.2e-8
2007	2.5e-7	8.1e-11	1.5e-6	4.8e-7	2.5e-5	4.5e-6	7.6e-7	1.5e-7	1.1e-5	3.8e-5	7.7e-9
2008	1.6e-7	7.0e-11	9.9e-7	3.1e-7	1.4e-5	2.9e-6	5.0e-7	9.9e-8	8.0e-6	2.5e-5	5.3e-9
2010	7.7e-8	5.1e-11	5.0e-7	1.5e-7	7.1e-6	1.4e-6	2.4e-7	4.6e-8	4.5e-6	1.2e-5	3.0e-9
2012	4.1e-8	3.7e-11	2.2e-7	8.5e-8	4.1e-6	7.5e-7	1.3e-7	2.8e-8	2.4e-6	5.6e-6	1.8e-9
2014	2.4e-8	2.7e-11	1.0e-7	4.9e-8	2.0e-6	4.1e-7	.3e- 8	1.7e-8	1.4e-6	3.1e-6	1.2e-9
2016	1.4e-8	2.0e-11	4.7e-8	2.8e-8	1.2e-6	2.1e-7 💉	3.4e-8	1.0e-8	7.5e-7	1.7e-6	7.3e-10
Odour Threshold	0.7	3.0e-4	3.7e-3	4.6e-4	1.0e-4	2.0e-2	2.0e-4	1.4e-4	0.7	0.54	*
1% of EAL	6.4e-4	*	*	1.3e-4	1.4e-3 🔗	1+211,	1e-4	*	1.9e-2	4.4e-2	1.6e-4

*No Standard Available

In all cases the predicted individual trace gases were below 1% of the EAL's taken from the EA's H1 Guidance and were well below the associated odour thresholds.

Recent gas monitoring of Area 6 (JBA, April 2004, see Appendix H) was undertaken and the values recorded for the odorous trace gases were found to be below the default values already modelled using GasSim, with the exceptions of dimethyl sulphide (recorded at 0.07mg/m³), limonene (2.5mg/m³), toluene (1.1mg/m³), xylene (0.009mg/m³) and benzene (0.93 mg/m³). To provide a more conservative prediction, the default values for the odour suite were replaced with these monitoring levels for the above trace gases and the model was re-run. Again in all cases the predicted trace gases were predicted below the associated thresholds at receptor 1. Therefore odorous trace gases should pose no significant risk to human health and cause no nuisance.

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Receptor	2 –	Residential	Housing	near	Area	6
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		Predict	ed Trace	Gas Con	centratio	ns (mg/m	3) at Rece	ptor 2			
	Carbon Disulphide	Diethyl Dísulphide	Dimethyl Sulphide	Ethanethiol	Hydrogen Sulphide	Limonene	Methanethiol	Propanethiol	Toluene	Xylene	Benzene
2005	1.3e-7	6.3e-11	6.7e-7	2e-7	1.3e-5	2.3e-6	4.3 e -7	7.9e-8	6.2e-6	2e-5	2.6e-9
2006	3.2e-7	6.1e-11	1.7e-6	6e-7	3e-5	5.5e-6	1e-6	1.9e-7	1.6e-5	4.8e-5	7.3e-9
2007	1.9e-7	5.3e-11	1.1e-6	3.8e-7	1.9e-5	3.4e-6	5.8e-7	1.2e-7	8.5e-6	2.9e-5	4.7e-9
2008	1.3e-7	4.5e-11	7.8e-7	2.5e-7	1.1e-5	2.2e-6	3.9e-7	7.7e-8	6.2e-6	1.9e-5	3.2e-9
2010	6.6e-8	3.3e-11	4.1e-7	1.3e-7	6.1e-6	1.2e-6	2e-7	3.9e-8	3.7e-6	1e-5	1.8e-9
2012	3.7e-8	2.4e-11	1.9e-7	8e-8	3.8e-6	6.8e-7	1.1e-7	2.4e-8	2.2e-6	5.1e-6	1.1e-9
2014	2.3e-8	1.8e-11	9.5e-8	4.9e-8	1.9e-6	3.9e-7	3.9e-8	1.6e-8	1.3e-6	3.1e-6	7.0e-10
2016	1.4e-8	1.3e-11	5e-8	3.1e-8	1.2e-6	2.3e	3.7e-8	1e-8	7.8e-7	1.1e-6	4.4e-10
Odour Threshold	0.7	3.0e-4	3.7e-3	4.6e-4	1.0e-4	20e-2	2.0e-4	1.4e-4	0.7	0.54	*
1% of EAL	6.4E-4	*	*	1.3e-4	1.4e-3	5 *	1e-4	*	1.9e-2	4.4e-2	1.6e-4
* No Standard	Availab	le		ionpi	rpostired	<u></u>	·				

In all cases the predicted individual trace gases were below 1% of the EAL's taken from the EA's H1 Guidance and were well below the associated odour thresholds.

Recent gas monitoring of Area 6 (JBA, April 2004, see Appendix A) was undertaken and the values recorded for the odorous trace gases were found to be below the default values already modelled using GasSim, with the exceptions of dimethyl sulphide (recorded at 0.07mg/m³), limonene (2.5mg/m³), toluene (1.1mg/m³), xylene (0.009mg/m³) and benzene (0.93 mg/m³). To provide a more conservative prediction, the default values for the odour suite were replaced with these monitoring levels for the above trace gases and the model was re-run. Again in all cases the predicted trace gases were found to be below the associated thresholds at receptor 2. Therefore odorous trace gases should pose no significant risk to human health and cause no nuisance.

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Receptor 3 – Site Boundary

		Pr	edicted Tra	.ce Gas Cor	ncentrations	s (mg/m³) a	t Receptor	3			
	Carbon Disulphide	Diethył Disulphide	Dimethyl Sulphide	Ethanethiol	Hydrogen Sulphide	Limonene	Methanethiol	Propanethiol	Tcluene	Xylene	Benzene
2005	6.6e-6	4.9e-10	3.6e-5	1.0e-5	7.26-4	1.2e-4	2.3e-5	4.4e-6	3.3e-4	1.1e-3	3.3e-7
2006	2.0e-5	4.7e-10	1.1e-4	3.8e-5	1.96-3	3.6e-4	6.6e-5	1.2e-5	1.0e-3	3.1e-3	9.3e-7
2007	1.2e-5	4.0e-10	6.9e-5	2.3e-5	1.2e-3	2.1e-4	3.6e-5	7.3e-6	5.4e-4	1.8e-3	6.0e-7
2008	7.7e-6	3.4e-10	4.7e-5	1.5e-5	6.5e-4	1.4e-4	2.3e-5	4.7e-6	3.8e-4	1.2e-3	4.1e-7
2010	3.6e-6	2.5e-10	2.4e-5	7.3e-6	3.6e-4	6.6e-5	1.1e-5	2.2e-6	2.1e-4	5.8e-4	2.3e-7
2012	1.9e-6	1.8e-10	1.1e-5	4.0e-6	1.9e-4	3.5e-5	5.9e-6	1.3e-6	1.2e-4	2.6e-4	1.4e-7
2014	1.1e-6	1.4e-10	4.8e-6	2.3e-6	9.6e-5	1.9e-5	3.0e-6	8.1e-7	6.5e-5	1.5e-4	9.0e-8
2016	6.6e-7	1.0e-10	2.2e-6	1.3e-6	5.6e-5	9.9e-6	1.6e-6	4.7e-7	3.6e-5	8.0e-5	5.7e-8
Odour Threshold	0.7	3.0e-4	3.7e-3	4.6e-4	1.0e-4	32.0e-2	2.0e-4	1.4e-4	0.7	0.54	*
1% of EAL	6.4E-4	*	*	1.3e-4	1.4e-3	*	1e-4	*	1.9e-2	4.4e-2	1.16e-4
* No Standard Av	ailable	A ship	or inspection copyright of	hpuposes of	H. and or						
The shaded c	ells shc	w pred	icted le	vels that	at exce	ed asso	ociated	thresho	olds. T	he	

* No Standard Available

The shaded cells show predicted levels that exceed associated thresholds. The model predicts significant levels of hydrogen sulphide (greater than the odour threshold) between the years 2005 and 2012 at the nearest site boundary.

In all other cases the predicted individual trace gases were below 1% of the EAL's taken from the EA's H1 Guidance and were well below the associated odour thresholds.

Recent gas monitoring of Area 6 (JBA, April 2004, see Appendix A) was undertaken and the values recorded for the odorous trace gases were found to be below the default values already modelled using GasSim, with the exceptions of dimethyl sulphide (recorded at 0.07mg/m³), limonene (2.5mg/m³), toluene (1.1mg/m³), xylene (0.009mg/m³) and benzene (0.93 mg/m³). To provide a more conservative prediction, the default values for the odour suite were replaced with these monitoring levels for the above trace gases and the model was re-run. No further predicted trace gases were found to be above the associated thresholds.

To provide a more accurate simulation for predicted levels of hydrogen sulphide, the model was again re-run using the most recent monitoring results as outlined above.

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For this odorous gas levels were found to be less than detection at all locations. Therefore the detection level was input into the model to replace the GasSim default values, i.e. 1ppb for hydrogen sulphide (0.00142mg/m³). When modelling the on-site recorded level, predicted concentrations at the nearest site boundary were found to be well below the associated thresholds.

8.2 **Lateral Gas Migration**

Lateral gas migration was also modelled using GasSim. The model simulates lateral migration using a one dimensional flow model, which is emitted uniformly from all sides of the landfill. It uses an advection and dispersion equation to simulate the migration of gas through the landfill liner. Using the model the predicted lateral migration of landfill gas in relation to the nearest site boundary (to the east of the landfill) was investigated.

8.2.1 Bulk Landfill Gas

Concentrations of methane and carbon dioxide just outside the landfill boundary were calculated to be 383,000mg/m3 (52%) and 501,000mg/m³ (25%) respectively. However, at a distance of 12m from the proposed landfill methane concentrations become zero, and at a distance of 11m away carbon dioxide concentrations become zero. The nearest site boundary is approximately 20m from the edge of the proposed landfill position, and therefore there should be no significant risk to any potential future development from lateral migration. OWNET HON

8.2.2 Odorous Emissions

When considering odorous trace gases and benzene, the model predicted that for all species the concentration would be zero beyond 8m from the landfill boundary. Again there should be no significant risk to any potential future development from the lateral migration of odorous trace gases.

The output graphs showing the lateral migration of landfill gas are provided within Appendix G.

Irrespective of the above findings, the installation of the proposed venting measures should intercept any lateral migration of gas and disperse it into the atmosphere.

9 Summary of Air Dispersion Modelling

Risk assessment undertaken using the GasSim model indicates that the risks posed to housing development from the predicted generation of methane and carbon dioxide in the proposed engineered landfill are likely to be insignificant. Modelled receptor concentrations of these gases are significantly below accepted limits of explosion and asphyxiation, and therefore the risk to human health at the receptors is likely to be insignificant. The landfill engineering design is therefore regarded to provide a large safety margin in this respect.

Modelled concentrations of odorous trace gases and benzene generated by the landfill are unlikely to pose a significant problem for the residents of the nearby housing developments when considering public health and potential nuisance. However when considering odorous trace gas modelled at the nearest site boundary, significant volumes of hydrogen sulphide are predicted (i.e. greater than threshold levels) when using GasSim default source levels.

When the model was re-run using actual recorded values, all of the odorous trace gases and benzene were found to be well below threshold levels at the nearest site boundary. As this scenario provides a more accurate picture of site conditions, it is anticipated that there should be no significant risk to public health or public nuisance to any potential future development at the site boundary from odorous landfill gas.

It is recommended that gas monitoring is carried out monthly during the operational phase of the landfill to provide a safety margin during operations and to provide information for any further GasSim modelling work, if required. All model results assume passive venting of gas, however, it is understood that flares will be incorporated into the landfill design for the management of landfill gas. Therefore, should monitoring indicate a potential for flaring, the landfill flares can then be operated.

Reports

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10 Appendices

Appendix A Figure 2.2 Site Infrastructure Layout Appendix B **GasSim Input Parameters** Appendix C **GasSim Project Details** Appendix D Composition of 1980's to 2010 Waste Streams Appendix E Single Vent and Generated Landfill Gas Output Graphs Appendix F GasSim Trace Gas Default Inputs for Odorous Gas Appendix G Lateral Migration Graphs Appendix H **Monitoring Results**

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Reports

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Air Dispersion Modelling Report Engineered Landfill

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Appendix A

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Appendix B

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Table 1: GasSim input parame	eters		
Parameter	Value	Unite	lustification
	Talue	Onita	
Infiltration	Uniform (10,15)	mm/vear	Professional Judgement
Waste Input	65,000	tonnes	As confirmed with JBA (03/04/04)
% Waste in place capped	Always 75 then 100	%	Assumption
Masta Maistura Contant	-		
Wetness	1M/ot		Drefessional Judgement
Weste Depaitu	Vvel	t/m O	Professional Judgement (Londoim Depart)
Vaste Density		1/11/3	Assumed as standard required in landfill
	0.00001	m Im la	Assumed as standard required in landfill
	0.00001	m/s	From previous hydrogeological investiagtion
Waste Breakdown			
Domestic	Uniform (21,37.4)	%	Approx 28.2% of 65,000 tonnes
Commercial	Uniform (21,37.4)	%	Approx 28.2% of 65,000 tonnes
Industrial	Uniform (21,37.4)	%	Approx 28.2% of 65,000 tonnes
Inert	Uniform (7.7,15.4)	%	Approx 15.4% of 65,000 tonnes
Proportion to CO2	15.1	%	Based on gas monitoring visits
Proportion to CH4	30.3	%	Based on gas monitoring visits
Waste Composition &			Default values for 1980s to 2010 waste streams
Cellulose Decay Rates			Default values for 1980s to 2010 waste streams
			net
Landfill Characteristics		1.	J OL
Length N/S	190	m only	2 cells x 95m (LandSim report)
Length E/W	85	m _ & ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~	LandSim report
Area	16150	102 jir	
		be tool	
Сар	actil ⁰ at	er	
Layer 1 thickness	0.005	m	Info from JBA fax received 07/04/04
Layer 1 Hydraulic Conductivity	5臣-11	m/s	Info from JBA fax received 07/04/04
Layer 2 thickness	\$ 0.001	m	Info from JBA fax received 07/04/04
Layer 2 Hydraulic Conductivity	<u>م</u> 4.3E-19	m/s	Info from JBA fax received 07/04/04
Liner	1 Officit		
Laver 1 thickness	1	m	Info from JBA fax received 07/04/04
Laver 1 Hydraulic Conductivity	0.00000001	m/s	Info from JBA fax received 07/04/04
Laver 2 thickness	0.005	m	Info from JBA fax received 07/04/04
Laver 2 Hydraulic Conductivity	5F-11	m/s	Info from JBA fax received 07/04/04
Laver 3 thickness	0.002	m	Info from JBA fax received 07/04/04
Layer 3 Hydraulic Conductivity	4.3E-19	m/s	Info from JBA fax received 07/04/04
Biological Methane Oxidation	10	%	Suggested by DEFRA (GasSim Manual)

Air Dispersion Modelling Report Engineered Landfill

Appendix C

G:\Inter Divisional\4000043 CRH Blessington\15 Reports & Photographs\Reports\721128-OR- 23 1\Appendices\Appendix 3\4000043-OR-5C.doc © Mouchel Parkman 2005 **Project Details**

 Project name: Engineered Landfill

 Client: Roadstone Duban

 Model: G-Unter Divisional/4000/343 CRH Blessington/GesSim/Engineered Landfill.gss

 Model Date: 16/04/2004 16 14 53

 Comments:

 Initial Model

 Start Year : 2004

 Simulation Period : 20 years

Infiltration

UNIFORM(10.0, 15.0)

Justilication JBA Professional Judgement

Waste Input

Year	Amount Deposited [1]	Composition	% Waste in Place Capped
2004	UNIFORM(195E+04, 2 38E+04	 1980's - 2010 waste streams 	SINGLE(75)
2005	UNIFORM(3 90E+04, 4 77E+04	 1980's - 2010 waste streems 	SINGLE(100)
2006	SINGLE(0)	1980's · 2010 waste streams	SINGLE(100)
2007	SINGLE(0)	1980's - 2010 weste streams 🛛 🧟	SINGLE(100)
2008	SINGLE(0)	1960's - 2010 waste streams, $^{\circ}$	SINGLE(100)
2009	SINGLE(0)	1960's - 2010 waste streems	SINGLE(100)
2010	SINGLE(0)	1980's - 2010 waste streams	SINGLE(100)
2011	SINGLE(0)	1960's - 2010 waste streams	SINGLE(100)
2012	SINGLE(0)	1980's - 2010 waste streems	SINGLE(100)
2013	SINGLE(0)	1980's - 201 0 weste streems	SINGLE(100)
2014	SINGLE(0)	1980's - 2000 weste streams	SINGLE(100)
2015	SINGLE(0)	1980's 😪 2010 weste streams	SINGLE(100)
2015	SINGLE(D)	1980's - 2010 weste streems	SINGLE(100)
2017	SINGLE(0)	1950 > 2010 waste streams	SINGLE(100)
2018	SINGLE(0)	1980's - 2010 waste streams	SINGLE(100)
2019	SINGLE(D)	1680's - 2010 waste streams	SINGLE(100)
2020	SINGLE(0)		SINGLE(100)
2021	SINGLE(0)	💉 1980's - 2010 weste streams	SINGLE(100)
2022	SINGLE(0)	1960's - 2010 weste streems	SINGLE(100)

Justification:

Approximately 65000 tennes over 18 months starting 2004 as confirmed with JBA (03/04/04)

100% Cap at end of operational period

Just#ication: Assumed to be 75% until completion agreed with JBA

Waste Moisture Content

Wet Justification: Moisture content inputs based on professional judgement

Waste Density (t/m3): UNIFORM(0.6, 1.0) Professional judgement (Landsim Report)

Leachate Head [m]: SINGLE(1) Assumed standard in landfill

Hydraulic Conductivity [m/s]: SINGLE(0.00001) From previous hydrogeological investigation

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Page I

Waste Breakdown

2004 Domestic Commercial Industrial Inert

2005

Domestic Commercie: Industrial Inert

2006

Domestic Commercial Industrial Inert

2007

Domestic Commercial Industrial Inert

2008

Domestic Commercial Industrial Inert

2009

Domestic Commercial Industrial Inert

2010

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2011

Domestic Commercial Industrial Inerl

2012

Domestic Commercial Industrial Inert

2013

Domestic Commercial Industrial Inert

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2014

Domestic Commercial Industrial Ineri

2015

Domestic, Commercial Industrial Inert

2016

Domestic Commercial Industrial ोधसार

2017

Cornestic Commercial Industrial inert

2018

Domestic. Commercial Industrial Inert

2019

Domestic Commercial Industrial Inert

2020

Domestic Comanercial Industrial Inert

2021

Domestic Commercia⁵ Industrie Inest

2022

Domestic Commercial Industrial Inert

Justification: Split between COI with up to 10,000 tennes C&D (Inert)

UNIFORM(21.0, 37.4) UNIFORM(21.0, 37.4) UNIFORM[21.0, 37.4] UNIFORM(7.7, 15.4)

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Proportion to Carbon Dioxide [%] Justilication. Based on previous gas monitoring visits

Proportion to Methane [%] Justification Based on previous gas monitoring visits

Cellulose Decay Rates

	Dry	Average	Wel
Slow	SINGLE(0.013)	SINGLE(0.046)	SINGLE(0.076)
Moderate	\$INGLE(0.046)	SINGLE(0.078)	SINGLE(0 116)
Fast	SINGLE(0.076)	SINGLE(0.116)	SINGLE(0.694)
		(and a state of the first canaly .

Justilioscion. Default Value

Trace Gases

Source Gases

Carbon disulphide **Diethyl disulphide Dimethyl disulphide** Demethyl sulphide Ethanethic! (ethyl mercaptan) Hydrogen sulphide Limonene Metnanelhiol (methyl mercapten) Odour Units (Predicted) Propanethiol Sulphide, total simulations with H2S Sulphède, lotal simulations without H2S Toblene Xylene (all isomers)

Justification: Oetault Values for odour suite

Trace Gas Half-life (years) Justification: **Delauli** Value

Landfill Characteristics

Landfill Geometry

Length N/S [m] Length E/W [m] Area (m2)

Justification: Taken from LandSen Report

Engineered Controls Cap

Composite First Layer: Thickness [m] Hydraulic conductivity [m/s] Second Layer: Thickness [m] Hydraulic Conductivity [m/s]

SINGLE(0.005) SINGLE(0.00000000005)

SINGLE(0.001) SINGLE(4.3E-19)

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Concentration [mg/m3] LOGTRIANGULAR(0.01, 0.1, 11.0) LOGTRIANGULAR(0.01, 0.1, 11.0) LOGTRIANGULAR(1.00E-03, 2.00E-02, 2.60E+00) LOGTRIANGULAR(1.00E-03, 2.00E-02, 4.00E+01) LOGTRIANGULAR(1.00E-03, 1.00E-02, 6.00E+01) LOGTRIANGULAR(0.01, 0.01, 41.9) LOGTRIANGULAR(5.70E-04, 2.40E+00, 5.57E+03) LOGTRIANGULAR(5.70E-04, 2.40E+00, 5.57E+03) LOGTRIANGULAR(1.008-03, 1.00E-01, 2.40E+02) LOGTRIANGULAR(0.005, 0.01, 87.0) TRIANGULAR(\$ 000+04, 1.25E+05, 2.50E+05) LOGTRIANGULAR (0.2, 0.2, 2.1)

SINGLE(15.1)

SINGLE(30.3)

LOGTRIANGULAR (1.00E-03, 2.40E+00, 5.58E+03) LOGTRIN GULAR (5.00E-04, 8.00E-03, 3.50E+00) LOGTRUM GULAR (0.01. 0.1. 1250.0) LOOTEDANGULAR (1.00E-03, 1.00E-03, 6.18E+04) of copyright

NORMAL(4.11, 1.58)

SINGLE[190] SINGLE(85) 16150

10/01/2004 10:56:53

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Justification Thickness: Information provided by JBA Conductivity Information provided by JBA

Liner Double Composite First Layer: Thickness [m] Hydraulic Conductivity [m/s] Second Layer: Thickness [m] Hydraulic Conductivity [m/s] Third Layer: Thickness [m]

SINGLE(1) SINGLE(0.000000001)

SINGLE(0.005) SINGLE(0.00000000005)

SINGLE(0.002) SINGLE(4.3E-19)

Fourth Layer Thickness [m] Hydraulic Conductivity [m/s]

Hydraulic Conductivity [m/s]

SINGLE(0) SINGLE(1)

Justification: Thickness: Information provided by JBA Conductivity: Information provided by JBA

Gas Plant

Engine 2005 Justification	to 2024	10	•	Downtime [%]: SINGLE(0)	
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Not Justified	iui oluesig.		ton purequir		
-	Ain/Fuel ratio	Methane Destry	clibe Efficiency [%]	Hydrogen Destruction Efficiency [%]	
Engras	0.01	SINCER(D) A	ight	anararafa).	
Engines	Helphi (m) 3	Orflice Diameter	- [m]	Temperature (C) 20	
		TSelle			
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Fiere	non-combu	stion products		SINGLE(89)	
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Flare	non-combu	stion products		SINGLE(99)	
Dimethyl disul	lphide			an Wilstand Carline to	
Engine:	nan-combi,	istion products		SINGLE(\$9)	
Flare	non-combu	istion products		Single(99)	
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Hydrogen sulphide				
Engine:	non-combustion products		SINGLE(99)	
Flare	non-combustion products		SINGLE(99)	
Limonene			ONIOL EXON	
Engme.	non-compustion products		Single(99)	
FIARB	non-contoustion products		SINGLE(AA)	
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Enguie.	real-composition products		984012(97) 2840154004	
Claig. Odour Unite (Brodie	ted)		(3164/03/2444 (2327)	
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Engine	non-combustion products		SINGLE(99)	
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Sulphide, total simi	lations with H2S		, -	
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Engine:	non-combustion products		SINGLE(99)	
Flere	non-combustion products		SINGLE(99)	
Toluene				
Engine.	non-combustion products		Single(99)	
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Atmospheric Tempe	rature [*C]: 2D			
Pressure (mbars): 10	1.36			
Atmospheric Density	/ [g/m3]: 1293			
Potential Density Gri	adient (K/m): 0.009			
Washout Coefficient	: (s-1) : 0.0001			
Deposition Velocity ([m/s]: 0.01			
Terrain Type: Parkla	nd/Open suburbas			
Roughness Lengt	n (m): 0.5			
Effective Windspe	ed Coampent: 0.3			
all the second sec	a			
38A rose as provide	£1			
)dour				
Compound: Toluend	3			
Limit (mg/m3]: 1				
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Data Contactor and Advantages of the Second	and a second state of the	TREESED IN INC.		Page 6
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Lateral Migration

Bulk Gases Air Diffusion Coefficients Carbon Dioxide (cm2/s): SINGLE(0.1613) Methane (cm2/s): SINGLE(0.2192) Hydrogen (cm2/s): SINGLE(0.00001)

Not Justified

Geosphere Moisture Content [%]: SINGLE(10) Porosity [%]: SINGLE(45)

Default pasqu'il values

Trace Gases Ges Carbon disulphide Diethyl disulphide Dimethyl disulphide Dimethyl sulphide Ethanethio' (ethyl mercapian) Hydrogen sulphide Limonene Methanethicl (methyl mercepten) Odour Units (Predicted) Propenethial Sulphide, total simulations with H2S Sulphide, total simulations without H2S Toluene Xylene (all isomers)

Default Value

Global Impact

Bulk Gases Global Warming Potential Cerbon Dioxide (t): 1 Methane (t carbon dioxoide): 21 Hydrogen (t carbon dioxide): 0

Default Value

Ozone Depletion Potential	
Carbon Dioxide [t Irichlorolluoromethan	e]: 0
Methane [t trichlorodiuoromethane]: 0	-
Hydrogen (t trichlorofluoromethane): 0	

Default Value

Trace Gases		•
Gas	Global Warming Potential	Ozone Depletion Potential
Carbon disulphide	0	0
Diethyl disulphide	0	0
Dimethyl disulphide	0	Ó
Dimethyl sulphide	0	ŭ
Ethenethiol (ethyl mercapten)	0	0
Hydrogen sulphide	0	Q
Limonene	D	Q
Methanethicl (methyl mercaptan)	D	ġ.
Odour Units (Predicted)	Q	0
Propenethio	D	0
i inia transmaticitati (Ari-Arisingan Calarak generata Landik ya	16/04/2004 16 14:53	Hype 7

Air Diffusion Coefficient SINGLE(0.108) #UNDEFINED? SINGLE(0.0898) #UNDEFINED? SINGLE(0.1623) #UNDEFINED? #UNDEFINED?

150.

Sulphide, total simulations with H2S Sulphide, total simulations without H2S Toluene Xylene (all isomers)

Exposure

Scenario: Residential without Plant Uptake Year: 2004 Distance from boundary [m]: 0 Direction: North East Emissions to model: <None Selected> Gas Viscosity [N.hr/m2]: 0.000000005 Henry's taw constant: Soil Type: Loam Soil Organic Matter [%]: 5 Wind apeed above ground surface in emblant mixing zone [cm/s]:12 Depth below ground to contaminated source zone [cm]:1

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Building Characteristics	
Area of walls in living space [m2]:	188
Area of windows [m2]:	20
Area of Roor (m2):	74.1
Height of Living space [m]:	5.4
Air exchange rate (total exchanges per hour	r) 1
Perimeter of building [m]:	34.4 x ^{1/2}
Air pressure inside house [Pa]:	101321 🔊
Area of house walls in cellar [m2]:	6.88
Height of subfloor vold (m):	6 St are
Air pressure inside subfloor vold [Pa]:	2° 101325
Temperature inside house [C];	× 585
Floor resistance [NH/m3]:	27.0
Average height of at openings [m]:	tion et 1
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	instit.
Building Materials	ot the

Building Materials	FOL MISS		
Material	Total Porosity (cm3)cm3)	Air-filled porosity [cm3/cm3]	Thickness (m)
Hardcore	0.55	0.25	Q.1
Banding Sand	<u>g</u> ss	0.5	0.05
Concrete	<u>~00.068</u>	0.034	0.1
Insulating layer (floors)	0.9	0.9	0.05
Brick (external wells)	Q.5	0.25	0.1
Lightweight block (walls)	0.068	0.068	0.1
Insulating layer (walls)	0.9	Q.9	0.055
Plasterboard (ceiling)	0.068	0.068	0.0125
Insulating layer (roof)	0.9	0.9	0.1
Screed (over beam/block fic	xor) 0.068	0.068	0.05
Suspended limber floor	0.2	0.2	0.03

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Appendix D

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Reports

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